

BSC

Study Cover Sheet

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YUCCA MOUNTAIN PROJECT

Preliminary Wet Handling Facility Throughput Study

Informal Study

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003	10/31/2007	Reason for Revision: Issued to support LA. This revision includes HI-STAR DPCs and standardized process times. New Gantt chart and model are included to capture changes. Changed operating process to accommodate design and operational changes for STCs and aging overpacks.	J. Monroe-Rammsy <i>[Signature]</i> 10/31/07	R. Silva <i>[Signature]</i> 10/31/07	D. Tooker <i>[Signature]</i> 10/31/07	D. Rhodes <i>[Signature]</i> 10-31-07
002	03/27/07	Reason for Revision: Facility process has been documented in BFD's and facility layout has stabilized. Better understanding of process times and review of times performed by operations. New Gantt charts and model have been developed to capture changes. The document text has been completely rewritten to capture these substantive changes, and therefore, revision bars have not been used.	J. Monroe-Rammsy 03/27/07	R. Silva 03/27/07	D. Tooker 03/27/07	D. Rhodes 03/27/07
001	05/31/06	Reason for Revision: All throughput calculations in Rev 000 used fuel assembly capacity for PWR DPC as 32 and BWR DPC as 68. However, Assumption 3.2.3 for Rev 000 had fuel assembly capacities listed as 24 and 44 for PWR DPC and BWR DPC respectively. The error has been corrected in this revision and does not affect any results in the study or attachment.	A. Achudume 05/30/06	D. Rhodes 05/30/06	N/A	T. Mulkey 05/31/06
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## ACRONYMS

BFD	block flow diagram
BOD	<i>Basis of Design for the TAD Canister-Based Repository Design Concept</i>
BWR	boiling water reactor
CRCF	Canister Receipt and Closure Facility
CSNF	commercial spent nuclear fuel
CTM	canister transfer machine
DOE	U.S. Department of Energy
DPC	dual-purpose canister
GA	General Atomics
HLW	high-level (radioactive) waste
MTHM	metric tons of heavy metals
PWR	pressurized water reactor
SFTM	spent fuel transfer machine
SNF	spent nuclear fuel
STC	shielded transfer cask
TAD	transport, aging and disposal canister
TC	transportation cask
WHF	Wet Handling Facility

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## 1.0 INTRODUCTION

This study describes the development of a preliminary throughput estimate for the Wet Handling Facility (WHF). This study estimates the throughput for the WHF License Application design as of September 2007. This design freeze allowed for the development of the throughput study without having to accommodate for minor updates to the facility design and documentation leading up to the License Application. The preliminary throughput estimate was generated based on the WHF Block Flow Diagrams<sup>1</sup> (BFDs) and general arrangement drawings<sup>2</sup>.

As analyzed, the WHF is configured to receive, handle, and repackage bare commercial spent nuclear fuel (CSNF), where each fuel assembly will be handled directly and loaded into a transport, aging and disposal canister (TAD). Truck-based transportation casks containing bare CSNF and rail-based transportation casks containing dual-purpose canisters (DPCs) are the primary waste streams allotted for the WHF (Ref. 6.2.3, Section 5.1.1).

For design flexibility, the WHF will be designed to handle bare CSNF arriving in rail-based transportation casks. Rail transportation casks are not considered to be a primary waste stream. It is presumed that the utilities that can handle and load the relatively large and heavy rail casks have the capability to load TADs; therefore, they do not need to ship CSNF bare but would ship CSNF within TADs. Alternative cases were investigated that included three sizes of rail-based transportation casks containing bare CSNF, where these alternatives were used to assess the sensitivity of the facility to larger capacity bare-fuel transportation casks.

This preliminary study does not investigate throughput for low-volume waste streams. For example, the WHF is able to receive DPCs within aging overpacks that are delivered by a site transporter. Horizontal DPCs delivered from the aging facility on a site-based tractor-trailer can also be handled within the WHF. Neither of these waste streams are modeled. In addition, off normal scenarios involving CSNF which would be processed within the WHF are not specifically modeled or analyzed for their impact on throughput.

A summary of the processes modeled start with the receipt and preparation of the bare CSNF transportation cask or the DPC transportation cask. Receipt and preparation activities include inspection, venting, sampling, and unbolting the casks. For DPCs, the rail-based transportation cask is then transferred to the canister transfer room within the facility where the DPC is loaded into a STC for further processing. The DPCs are moved to a DPC cutting station where the outer lid (if used) and the inner shield lid welds are machined off. The DPC within the STC is placed into the pool and the inner shield lid is removed. The bare-fuel transportation casks are transferred directly from the preparation station to the pool for lid removal. Once the lid is removed from either the bare-fuel transportation cask or the DPC, the bare CSNF is transferred into the in-pool staging racks. (In actuality and outside of this model, the bare CSNF will most likely be transferred directly into a new TAD that has been pre-positioned in the pool; therefore, this model adds conservatism as discussed in Assumption 3.2.4.) Once the transportation cask or DPC is unloaded, the empty transportation cask or empty DPC within the STC is removed from the pool, drained, and prepared for export from the facility. A new TAD within an STC is loaded into the pool and the fuel from the racks is transferred to the TAD. The now loaded TAD is removed from the pool, drained, welded and dried. Once complete, the TAD is transferred to the cask unloading room. The TAD is transferred out of the STC and into an aging overpack and moved out of the facility to either the Canister Receipt and Closure Facility (CRCF) or to the Aging Facility (Ref. 6.2.11).

<sup>1</sup> Block flow diagrams include Revision 00A of the Level 2 and Draft Revision 00Bb of the Level 3 diagrams (Refs. 6.2.11, 6.2.12, 6.2.13, 6.2.14, 6.2.15, 6.2.16, 6.2.17, 6.2.18, 6.2.19, 6.2.20, 6.2.21, 6.2.22, 6.2.23, 6.2.24, 6.2.25, 6.2.26, 6.2.27, and 6.2.28)

<sup>2</sup> Site layout drawing include Revision 000 for the first and second floor and one elevation (Refs. 6.2.6, 6.2.8, 6.2.9 and 6.2.10)

The results of the preliminary throughput estimate are presented in terms of annual transportation cask processing capability, TADs produced and exported from the facility (sent to the CRCF or alternatively to the Aging Facility), and an estimate of total metric tons of heavy metal (MTHM) processed.

The preliminary results and conclusions presented in this study are based on simplifying assumptions (Section 3.2). Through the use of simplifying assumptions, results obtained are believed to be representative of the processing capabilities of the WHF. The calculated throughput rates do not represent exact or final results.

## 1.1 Purpose and Objectives

The purpose of this *Preliminary Wet Handling Facility Throughput Study* is to estimate the throughput capability of the preliminary WHF design based upon simplifying assumptions. The objective of this throughput estimate is to assist in design development and to provide initial conformance verification that the facility is capable of meeting the assigned processing rates (Criterion 3.1.1).

This study was developed in accordance with *Engineering Studies* and is classified as an informal study (Ref. 6.1.1, Section 2.2) and is within the scope of the contract as specified in the requirements documents (Ref. 6.2.3, Section 2.2.1.2). Per Section 2.1 of the *Engineering Studies* (Ref. 6.1.1) procedure, the results of this informal study are considered preliminary.

## 1.2 Scope

This preliminary throughput estimate only investigates those operations occurring within the WHF. Processes outside of the WHF (i.e., rail and truck staging, site transporter delivery and export, etc.) may or may not affect the facility throughput capability. To determine WHF throughput capability without assessing outside factors, it is assumed that all processes that are inputs to or outputs from the facility are available on demand. All WHF process inputs, such as loaded transportation casks and new TADs, are assumed to be immediately available when required. All model outputs, such as empty casks and loaded TADs, are assumed to be immediately removed when made ready (see Assumption 3.2.1).

## 2.0 RESULTS AND CONCLUSIONS

The preliminary results and conclusions presented in this report are based on the simplifying assumptions provided in Section 3.2. Through use of the simplifying assumptions, the results obtained are believed to be representative of the processing capabilities for the WHF design as of September 2007.

While an operations review was performed, operations activities are not wholly addressed or captured in these throughput estimates and may impose increased operational times for each of the processes. This poses a significant risk in the estimation of the throughput. Thus, the calculated throughput rates do not represent exact or final results. The results should be used as preliminary input for design development. Future evaluation should be conducted to ensure the validity of the conclusions.

## 2.1 Results

The model results are considered optimistic, and per Assumption 3.2.1, outside factors are not represented in the WHF model specifically. While not specifically known, it is anticipated that the outside factors will degrade the performance of the WHF. The primary outside factors include sequencing the delivery of trucks from truck staging, railcars from rail staging, export of TADs

within aging overpacks to either the CRCF or Aging Facilities, delivery of empty TADs, and arrival of site transporter from the Receipt Facility and the Aging Facilities.

Table 1 presents a summary of the throughput model results. For full documentation of throughput model results, refer to Section 5.1.

Table 1. Summary of Throughput Model Results

Scenario	Model Results		
	TADs Produced <sup>a</sup>	Transportation Casks <sup>b</sup>	MTHM <sup>c</sup>
Truck Only	36	191-192	309-315
DPC Only	46-47	44-46	410-418
Mix of Truck and DPC	40-52	61-147	363-464
Small, Med, Large Rail Bare CSNF	54-74	60-138	461-627

Notes: <sup>a</sup> See Table 4 <sup>b</sup> See Table 6 <sup>c</sup> See Table 5

Criterion 3.1.1 requires the WHF to be able to process a combined 307 MTHM per year. The results presented in Table 1 show that the WHF meets the throughput requirement for waste streams containing truck only, mix of truck (bare-fuel) and DPC transportation casks, and DPC only cases.

In addition to the 307 MTHM per year requirement, a design goal of 40 TADs per year has been informally established<sup>3</sup>. The results in Table 1 show that the WHF currently does not meet the design goal for a waste stream consisting of a truck-only waste stream.

## 2.2 Conclusions

A primary purpose for performing throughput analyses is to understand which processes and systems impede the flow of materials through the facility; i.e., which processes are the bottlenecks. The results discussed in Section 5.2 showed that no single piece of equipment is over utilized; however, a bottle neck exists with the preparation station #1 as discussed in Section 5.2.3. The primary impedance to facility throughput is the layout and flow of the objects through the facility—specifically through the preparation station #1. This is visually apparent by reviewing Figure 2 as discussed in the concept of operations in Section 4.2.

Discussed in Section 5.2.1, the secondary impedance to facility throughput is the overhead cranes, which are the primary conveyance through the WHF. To avoid interference between the cranes or spent fuel transfer machine (SFTM), only one crane or SFTM is allowed to operate at a time within a particular zone. No two loaded cranes or SFTM can occupy the same zone or pass through a zone as another loaded crane. Simply, one crane has to wait for the other to complete its job prior to operating. This inability to move across zones and pass-by each other restricts the crane movements and utilization.

## 2.3 Recommendations for Future Work

The following are recommendations to improve the WHF layout and design (Section 2.3.2), as well as recommendations to improve the fidelity of the model and the veracity of the results (Section 2.3.1).

<sup>3</sup> A BWR TAD contains 44 fuel assemblies. At 0.174 MTHM per assembly (Assumption 3.2.10) for forty BWR TADs equates to approximately 306 MTHM. A PWR TAD contains 21 fuel assemblies. At 0.433 MTHM per assembly (Assumption 3.2.10) for forty PWR TADs equate to approximately 364 MTHM.

### 2.3.1. Recommendations for Throughput Model Improvement

As the design progresses, re-evaluation of the throughput will be required. Changes to the facility layout and operations are inevitable in this preliminary design phase and will need to be captured in future versions of the throughput model.

For the development of the throughput estimate, the Gantt charts form the basis of the throughput model. Parallel operations within the WHF were captured in the Gantt charts at the third-level of the BFDs. However, the Gantt charts break down each level-three BFD step into numerous individual process steps at the fourth-level. Parallel activities are captured at this level but only under the third-level operation. Parallel activities at the fourth-level do not span across level-three BFD process steps. By performing future detailed analysis of each operational step, parallel activities at the fourth-level that span across the level-three BFD operations could be discovered and incorporated in future versions of the Gantt charts and subsequent throughput models. While parallel activities at the fourth-level will likely have only minor effects on the individual level-three BFD times, the aggregate sum of the small improvements to the process should improve the overall throughput results.

While operations reviewed the WHF Gantt charts, specific and detailed feedback was not received. General, high-level comments were incorporated; however, specific details pertaining to actual process and process times were not fed back for incorporation. The next revision of the throughput evaluation should incorporate specific, detailed operations input, which may impose increased operational times for each of the processes. This imposes risk in the throughput estimation.

To help balance and mitigate risks from operations inputs, future literature searches will continue to be performed to try to further discover published operational times from actual fuel handling operations. The use of these analogs will help establish credibility for the assumed process times captured in the Gantt charts.

Capabilities of the preliminary WHF throughput model can be further utilized or enhanced in the following areas to provide additional information as needed:

#### Waste Stream Variations

- Perform longer model runs (accounting for backlog)
- Transportation effects (truck, rail, site transporter, and STC variations)

#### Facility Optimization

- Process sequence variation
- Bottleneck identification

#### Development of Operational Data

- Better equipment utilization data (e.g., crane, welding equipment, SFTM, canister transfer machine, etc.)
- Cumulative process timing to support worker dose rate determinations
- Capture of detailed operations activities and their effects on process times

#### Model Fidelity

- Better process differentiation between transportation cask type and the related transportation cask operations, as well as, STC and site transporter operations
- Better process modeling of the horizontal DPCs, such as the MP-187/197 transportation casks (Refs. 6.2.39 and 6.2.40)

- Welding operational differences for pressurized water reactor (PWR) and boiling water reactor (BWR) TADs
- Identification of cask cooling requirements, process times, and frequency of occurrence (Assumption 3.2.30).

### 2.3.2. Recommendations for Wet Handling Facility Improvement

Discussed in Section 5.2, the use of preparation station #1 has been shown to be the facility bottleneck. The flow of objects through the facility and the location of the preparation, DPC cutting, and welding stations needs to be reevaluated and could potential improve the facility throughput. The circular flow of TADs through the facility is disrupted by the facility layout and by the requirement to export all TADs within an aging overpack. The reevaluation of material flow through facility should include the primary cranes as they are the main conveyance of objects through the facility and have a direct impact on the overall facility throughput.

## 3.0 STUDY BASES

### 3.1 Criteria

- 3.1.1 The WHF shall be designed to be capable of receiving 230 MTHM per year of bare CSNF from legal weight trucks, over-weight trucks and rail based bare fuel casks, as well as, 77 MTHM per year of CSNF in DPCs by rail. In the event that the DOE determines that rail access to the repository site will be unavailable to support system operating conditions and receipt rates, the previous acceptance rates will not apply and will, instead, be based on the availability of truck transportation capability (Ref. 6.2.3, Section 5.2.1.2)
- 3.1.2 The WHF shall be designed to receive the following transportation cask designs (non-exclusively) (Ref. 6.2.3, Section 5.2.1.1.4):
- |           |                           |
|-----------|---------------------------|
| • GA-4    | • MP-197                  |
| • GA-9    | • HI-STAR 100             |
| • NAC-LWT | • TranStor TS-125         |
| • NAC-STC | • TN-68 TSC               |
| • NAC-UMS | • TAD Transportation Cask |
| • MP-187  |                           |
- 3.1.3 The capacity of the TAD canister shall be either 21 pressurized water reactor (PWR) spent fuel assemblies or 44 boiling water reactor (BWR) spent fuel assemblies (Ref. 6.2.3, Section 33.2.2.3).
- 3.1.4 The TAD canister shall be designed to facilitate helium leak testing of closure features (Ref. 6.2.3, Section 33.2.2.36-b).
- 3.1.5 Closure welds shall be used for TAD canister containment in accordance with standard nuclear industry practice (Ref. 6.2.3, Section 33.2.2.36-a).
- 3.1.6 In accordance with industry standards and regulatory guidance, the TAD canister shall be designed to facilitate the following (Ref. 6.2.3, Section 33.2.2.39):
1. Draining and vacuum drying to remove water vapor and oxidizing material.
  2. Filling with helium to atmospheric pressure or greater as required to meet leak test procedural requirements.

3. Sampling of the gas space to verify helium purity.
  4. Limiting maximum allowable oxidizing gas concentration within the loaded and sealed TAD canister to 0.20 percent of the free volume in the TAD canister at atmospheric pressure.
- 3.1.7 The loaded aging overpack shall be designed to be moved to the aging pad via site transporter using a pair of lift beams (e.g., forklift) (Ref. 6.2.3, Section 33.2.4.24).
- 3.1.8 The WHF shall provide for the removal or retraction of personnel barriers from around the cask while in the preparation areas (Ref. 6.2.3, Section 5.2.2.3.10).

### 3.2 Assumptions

The preliminary results and conclusions presented in this study are based on the following simplifying assumptions. Through the use of these simplifying assumptions, results obtained are believed to be representative of the processing capabilities of the WHF. The process times and detailed operations are based upon knowledge of the process, basic understanding of process times and understanding of analog processes. Several of the following assumptions are justifications for process times and were reviewed by operations. Some processes within the WHF were undetermined and engineering judgment could not be generally applied. These processes need further analysis to establish reasonable process times. While not inclusive to all processes, those processes requiring further investigation are captured within these assumptions and include the basis for the particular process time.

- 3.2.1 **Assumption:** On demand delivery conditions were used in the throughput model. All inputs, such as loaded transportation casks and new TADs, were available when required. All outputs, such as empty transportation casks, empty DPCs, and loaded TADs, were removed when ready.

**Rationale:** The scope of this informal engineering study was limited to the WHF. Processes outside of the WHF (e.g., rail and truck staging, STC movement, aging, remediation activities, etc.) may or may not affect the facility throughput capability. To determine WHF throughput capability without outside factors, it was assumed that all processes that were inputs to or outputs from the facility were available on demand. Therefore, for the scope of WHF only, this assumption is suitable for use in this preliminary engineering study.

**Used in:** This assumption was used in the development of the throughput model (Attachment I), in the WHF Gantt chart (Appendix A), and is discussed in Section 5.2.

- 3.2.2 **Assumption:** To estimate the annual throughput capability of the WHF, all calculations were performed using steady state conditions. Ramp-up and ramp-down times, as well as facility startup activities, were not included.

**Rationale:** Facility operational capability will ultimately be affected by startup activities. However, for study simplification, ramp-up and ramp-down times have not been established and, therefore, were not incorporated.

In addition, facility operational capability is characterized as representing some significant maturity of operations that may not be realized at startup. During initial operations, minor modifications may be made to the facility and/or procedures that do not affect the safety basis of the facility but may increase productivity and subsequent throughput. This assumption is suitable for use in this preliminary engineering study.

**Used in:** This assumption was used in the development of the throughput model (Attachment I), in the WHF Gantt chart (Appendix A), and is discussed in Section 5.2.

- 3.2.3 **Assumption:** For the purposes of this preliminary throughput study, facility availability was assumed to be 75 percent. The 25 percent non-availability was used to account for routine maintenance and equipment failures, off-normal operations, and recovery time.

**Rationale:** The facility was assumed to be available to operate 24 hours a day, 7 days a week. For this version of the throughput study, 75 percent facility availability was assumed. This is equivalent to three months down time per year which could consist of one month planned outage and two months for unplanned outages.

In addition, this throughput study did not simulate failure rates of equipment. Failure modes and effect analyses, subsequent failure rates, and mean time to repair data were assumed to be accounted for in the 25 percent unavailability factor.

As the design progresses and better definition is available for specific equipment types, failure rates and recovery times, system redundancy features, operating procedures, and waste processing requirements, the facility and equipment availability will be reviewed and better quantified. Therefore, this assumption is suitable for use in this preliminary engineering study.

**Used in:** This assumption was used in the development of the throughput model (Attachment I), and in the WHF Gantt chart (Appendix A).

- 3.2.4 **Assumption:** All CSNF assemblies are transferred from the transportation cask or DPC to the in-pool racks prior to being placed into a TAD.

**Rationale:** To reduce in-pool residence time for the TADs and to implement software routines and subsequent logic for the throughput model, an operational philosophy was assumed for the WHF where the facility will receive any type of awaiting transportation cask, regardless of the transportation contents or type, and process that cask type. This is independent of the TAD type within the pool (if any). All fuel from the arriving transportation cask or DPC is conservatively assumed to be transferred to the in-pool storage racks rather than directly to an awaiting TAD. This portion of the model is considered a "Push" model, as the transportation casks are pushed into the facility regardless of type.

Alternatively, the in-pool racks operate on a "Pull" model. That is, the model requests a TAD type (PWR or BWR) based on the rack contents, and not on the incoming waste stream. The logic for requesting a TAD type is based on the quantity of fuel assemblies in either the PWR rack or the BWR rack. The model uses the fuel rack contents to calculate the integer number of TADs that could be created from the two fuel types.

For example, if the model has recently processed two PWR DPCs, one BWR DPC, and three BWR truck casks, then the PWR racks would contain 64 PWR (32x2) fuel assemblies and 95 BWR (68 + 3x9) fuel assemblies. Based on the rack contents, the logic would request a PWR TAD. While there are more BWR fuel assemblies in the rack, there is only enough to create two BWR TADS. Alternatively for this example, there are 68 PWR fuel assemblies, which is enough to create three PWR TADS. Since the fuel racks contain more PWR TADS than BWR TADS, the model requests or "pulls" a PWR TAD for the next loading operation. The purpose for this logic-methodology is two-fold.

First, this methodology reduces in-pool residence time of TADs. It is advantageous to reduce the in-pool residence time to minimize contamination of the external TAD. Prior to loading into the pool, borated water is put into the annular space between a TAD and the STC. A rubber gasket or seal is then inserted in the annulus. This helps prevent any in-pool contaminants that have not been filtered out of the pool water from coming in contact with the TAD exterior. The sides of the TAD are not accessible for washdown or further decontamination. The longer the TAD resides in the pool, the greater the chance that possibly contaminated pool water will infiltrate the rubber

gasket and mix with the clean borated water within the annulus. This methodology places a STC/TAD into the pool only if there is enough fuel in the racks to completely load the TAD. Alternately, if the TAD were placed in the pool before a truck cask were delivered, then the TAD would reside in the pool for several truck deliveries before being completely loaded, spanning multiple days. Placing the TAD into the pool only when there is adequate fuel for immediate fuel transfer expedites the TAD loading and subsequent removal from the pool.

Second, this logic-methodology prevents the facility from becoming "locked-up". The software must follow specific "if-then" rules and cannot use any higher-level, cognitive algorithms and is therefore confined by these if-then rules.

If the model logic were set-up to request a TAD canister based on the transportation cask type, then it is feasible that the facility will enter a locked state, which was observed during model development. In this scenario, if a PWR truck cask entered the facility then the model logic would request a PWR TAD. All four fuel assemblies from the PWR truck cask would be transferred to the PWR TAD, and not to the in-pool racks. It requires six PWR transportation casks containing four assemblies each to fill a 21 assembly PWR TAD, with three extra fuel assemblies being placed in the fuel racks at the end of the campaign. However, it is not guaranteed that the next transportation cask in the incoming facility queue is PWR truck cask.

To continue with this example, lets assume that a BWR truck cask is next in line and the PWR TAD within the pool still contains only four fuel assemblies. The nine fuel assemblies within the BWR truck cask must be transferred to the fuel assembly racks as the TAD is of the wrong type. Now, if a BWR DPC is next in the processing queue, all 68 fuel assemblies would be transferred to the rack as well. This string of BWR casks could continue until the entire BWR fuel rack would become full (Assumption 3.2.5). If another BWR truck cask or DPC is in the queue before the PWR TAD is completely filled, then the facility can not process any more fuel and is effectively "locked up". With both the BWR rack full and with a PWR TAD partially full within the pool, the software does not have the capability to correct and recover from this situation.

Designing the software logic to choose the TAD-type based on the quantity of fuel assemblies within the rack, and not on the transportation cask type being processed, allows the TADs to be filled regardless of which type of transportation cask is next and the facility can never enter a locked-state. Therefore, the model is set up to put all fuel assemblies in the rack and "pull" the specific TAD for the process. Thus, all fuel assemblies go to the in-pool rack prior to being loaded into a TAD.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

**3.2.5 Assumption:** Once either the PWR or BWR racks contain 132 fuel assemblies, transportation casks are prevented from entering the facility and are held within the rail or truck buffer area.

**Rational:** Assumption 3.2.4 effectively separated the transportation cask processing from the TAD loading and closure operations. This allows for transportation casks to be processed at the same time as a TAD is being welded and dried—a relatively lengthy process. To prevent the PWR and BWR fuel assembly racks within the pool from exceeding a maximum of 200 fuel assemblies each, transportation casks are not allowed within the facility once either rack reaches 132 fuel assemblies. TAD closure operations are not affected by this logic and will continue to process TADs. Once the number of fuel assemblies within each rack drops below 132, then transportation casks are then allowed to enter the facility.

The cut-off number (132) was selected as it is the rack capacity (200) subtracting one BWR DPC (68). Based on this assumption, the model stops incoming transportation casks from entering once the racks reach 132. It is possible that another cask is currently being processed within the

facility. The worst case is that a 68-BWR DPC is being cut-open. The in-pool rack has to have the capacity to handle this situation, and is thus reserved 68 spaces.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

- 3.2.6 **Assumption:** The WHF concept of operations is assumed to be a step-wise, sequential process where items will move from station to station. And, once a station becomes available another item will move into that station. This process allows for multiple truck casks, DPCs, and TADs to be processed simultaneously, significantly improving the parallel operations within the facility.

**Rationale:** Previous revisions of the WHF throughput engineering studies only allowed a single truck cask or DPC to be processed at a time. For example, a truck cask would enter the facility, be prepared for unloading, move into the pool, fuel unloaded from the cask, the cask moved back to a preparation area, the cask dried and prepared to leave the facility, loaded back onto the same conveyance which brought the cask, and exported from the facility. Only then would another truck cask be able to enter the facility and be processed.

With this revision of the throughput study, the operational philosophy has been changed to a "round-robin" scheduling methodology. With this methodology, more than one transportation cask, DPC, and TAD can be processed simultaneously as each object flows through the facility. In general, this process flows circularly from the conveyance on the east side of the building, to the north side of the building for preparation operations, to the pool on the west for loading/unloading operations, to the southern side for exit and welding operations, and back to the conveyance on the east side.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

- 3.2.7 **Assumption:** The assumed capacity of a truck transportation cask is nine BWR CSNF assemblies or four PWR CSNF assemblies.

**Rational:** For this study, all truck-based transportation casks are assumed to be either the PWR or BWR variants of the General Atomics (GA) truck casks, referred to as the GA-4 or the GA-9, respectively (Ref. 6.2.30, Section 1.1 and Ref. 6.2.31, Section 1.1). Interestingly, the GA-9 is capable of handling either 4 PWR or 9 BWR CSNF assemblies (Ref. 6.2.31, Section 1.1 and Ref. 6.2.32, Section 1.1), whereas the GA-4 can only handle 4 PWR assemblies.

Per the *Basis of Design for the TAD Canister-Based Repository Design Concept*, referred to as the BOD, (Ref. 6.2.3, Section 5.2.1.1.4), the WHF will also be designed to handle the NAC International Legal Weight Truck (NAC-LWT) transportation cask (Criterion 3.1.2), which can transport either two BWR CSNF assemblies or a single PWR CSNF assembly (Ref. 6.2.34, p. 1.1-1). However, the data<sup>4</sup> from the *2002 Waste Stream Projections Report* (Ref. 6.2.29) for a 10 year old fuel first scenario does not contain any shipments made with a NAC-LWT. This does not preclude the use of a NAC-LWT; but rather, based on the low capacity of the cask type, it is assumed that the NAC-LWT will be a relatively small proportion of the waste stream and is therefore not utilized in this throughput analysis.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

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<sup>4</sup> For the data from the *2002 Waste Stream Projections Report* (BSC 2003), see Attachment I, file "Waste Stream Evaluation.xls", tabs "BWR Data Only" and "PWR Data Only"

**3.2.8 Assumption:** Two processing rates were assumed for handling DPC transportation casks—one process time for the HI-STAR 100 and a second process time for all other variants of DPC transportation casks, referred to as a generic DPC. There was no time differentiation in the DPC transportation cask handling processes between the various generic transportation cask types.

**Rational:** All transportation cask variants required in Criterion 3.1.2 for the DPC waste stream are assumed to be prepared for unloading and exported from the facility utilizing a similar process and timeframe, with exception of the HI-STAR 100. The HI-STAR 100 requires a slightly different process for unloading from the railcar than a generic DPC. In addition, the HI-STAR 100 requires a slightly different process for loading the empty HI-STAR 100 back onto the railcar.

The process time to transfer each of the fuel assemblies out of the respective DPC, either HI-STAR 100 or generic, is captured. For example, a DPC transfer is a single operation and is modeled as such. However, the transfer of the DPC fuel contents (i.e., the CSNF) is modeled individually and accounts for the number of PWR or BWR fuel assemblies. It is the transportation cask preparation and handling process that is generically modeled as an assumed cask (Table 2). Until specific operational sequences, cask quantities (waste stream), and process times are established for each transportation cask type, this assumption is suitable for use in this preliminary throughput study.

Table 2. DPC Transportation Cask Information

DPC Transport Cask	Max Capacity		Number of Lid Bolts (Inner/Outer)	Number of Lids	Impact Limiter Bolts (Per Impact Limiter)
	BWR	PWR			
<sup>1</sup> MP-187	0	24	36	1	12
<sup>2</sup> MP-197	61	0	48	1	12
<sup>3</sup> HI-STAR 100	68	32	54	1	10
<sup>4</sup> NAC-STC	0	36	36/42	2	16
<sup>5</sup> NAC-UMS	56	24	48	1	16
<sup>6</sup> TS-125 (TranStor)	74	21	60	1	12
<sup>7</sup> TN-68	68	0	48	1	<sup>b</sup> 13
<b>Assumed Cask</b>	<b>68</b>	<b>32</b>	<b>48</b>	<b>1</b>	<b>16</b>

Notes: <sup>a</sup> Partial list as specified in Criterion 3.1.2  
<sup>b</sup> Impact limiters are attached using 13 individual Tie Rods. See Ref. 6.2.38, Drawings 972-71-2 and 972-71-3

References:<sup>1</sup> Ref. 6.2.39, pp. 1.1-3, 1.1-4, and General Arrangement Sheet 1  
<sup>2</sup> Ref. 6.2.40, Dwgs. 1093-71-1, 1093-71-2, 1093-71-3, 1093-71-11.  
<sup>3</sup> Ref. 6.2.33, pp. 1.1-1, and Drawings. 3913 Sheet 5 and C1765 Sheet 5  
<sup>4</sup> Ref. 6.2.35, pp. 1.1-1, 1.1-2, 1.2-5, 1.2-6, 1.2-9  
<sup>5</sup> Ref. 6.2.36, pp. 1.1-1, 1.2-4  
<sup>6</sup> Ref. 6.2.2, pp. 1.2-5, and Drawings. FS-200 Sheets 2 and 3  
<sup>7</sup> Ref. 6.2.38, Drawings 972-71-1 through 972-71-10

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

- 3.2.9 **Assumption:** Estimated process times, as presented in the Gantt charts (Appendix A), were assumed to be reasonable for the stated processes.

**Rationale:** A formal time and motion study for the CSNF processing within the WHF was not performed. The process times and detailed operations are based upon knowledge of the process, basic understanding of process times and understanding of analog processes. It is anticipated that the processing times and steps will be further defined and reviewed as the facility design matures, and will be subsequently incorporated into future revisions of the facility throughput model.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

- 3.2.10 **Assumption:** The average MTHM per PWR and BWR fuel assembly is 0.433 and 0.174, respectively.

**Rationale:** The actual MTHM per fuel assembly varies. The average MTHM per fuel assembly is calculated from the data provided with the *2002 Waste Stream Projections Report* (Ref. 6.2.29, Section 3.2 and Table 2) for the 70,000 MTHM case where the 10-year old fuel is sent to the repository first. This data is found in (Attachment I), Excel file "Waste Stream Evaluation", Tabs "PWR Data Only" and "BWR Data Only".

**Used in:** This assumption was used in the estimation of MTHM for Table 5 calculated from the throughput results presented in Attachment I.

- 3.2.11 **Assumption:** Personnel Barriers are not removed within the WHF.

**Rationale:** Currently, the WHF is required to have the provision to remove personnel barriers (Criterion 3.1.8). However, the specific location where they are to be removed has been in debate, either within the WHF or another location within the repository operations area, such as the security station. The current operational philosophy is to have all personnel barriers removed at the security station and not within the WHF. Until a definitive decision is made for the location where personnel barriers are to be removed, it is reasonable to assume that they will be removed at the security station.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

- 3.2.12 **Assumption:** All casks are washed prior to entering the WHF.

**Rationale:** Currently, there is no formally defined location where STCs and transportation casks will be washed. Washing is required to remove the majority of road dirt from the external surfaces of the respective cask, which will help prevent the introduction of dirt or other contaminants into the pool environment. Currently, this wash-down is expected to occur somewhere outside of the WHF, rather than within the decontamination pit.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

**3.2.13 Assumption:** New TADs that will be loaded with CSNF within the WHF are brought into the facility by means of an STC. Once the loaded and welded TAD is transferred to an aging overpack, the empty STC is sent out of the WHF to the Warehouse and Non-Nuclear Receipt Facility for loading with another new TAD.

**Rationale:** At the time of development for this version of the throughput study, the use of STCs was undergoing reevaluation. A design change required that all loaded TADs exit the facility through aging overpacks. However, it was unclear if the STC, which was used during the preparation, loading, and closure of the TAD canister would be allowed to leave the facility. For use in this throughput only, it was assumed that a STC loaded with a new TAD or an unloaded STC could enter and leave the facility with appropriate contamination surveys.

**Used in:** This assumption was discussed in Section 4.2, used in the development of the throughput model (Attachment I), and used in the WHF Gantt charts (Appendix A).

**3.2.14 Assumption:** The universally used STC has 48 lid bolts that require 5 minutes each to install, 3 minutes each to remove.

**Rationale:** The NAC-UMS Storage System, which is similar in size and function to a TAD based STC, utilizes 48 Bolts (2 inches in diameter x 8.5 inches long) weighing approximately 30 pounds each (Ref. 6.2.36). Thus to remove each bolt, it will take approximately 3 operators 3 minutes each to remove—one person operating the impact wrench, one person to support and catch the bolt, and a third person to stack the bolts on the rack. Thus to remove all STC lid bolts, it will take

$$3 \text{ min} \times 48 \text{ bolts} = 144 \text{ minutes} = 2.4 \text{ hours} \quad (\text{Eq. 1})$$

To install the STC lid bolts it will take approximately 3 operators, 3 minutes each to run-in the bolt, and two minutes each to torque the bolts to specification and torque pattern. Thus to install all lid bolts, it will take:

$$5 \text{ min} \times 48 \text{ bolts} = 240 \text{ minutes} = 4 \text{ hours} \quad (\text{Eq. 2})$$

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

**3.2.15 Assumption:** The universally used STC will require only 4 lid bolts when an STC is moved within the facility, where each bolt requires 5 minutes to install, 3 minutes to remove, or 5 minutes to install or remove underwater.

**Rationale:** To prevent fuel ejection from an off-normal tip-over/drop event, it is assumed that four lid bolts will prevent the lid from opening and ejecting fuel assemblies.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

**3.2.16 Assumption:** The universally used STC will have a permanent lid lifting device either built into or attached to the STC lid.

**Rationale:** The STC is not yet designed. The operations require the STC lid to be removed and installed by a crane and grapple; thus, the lid will require a lid lifting device. While the specification for the Aging Overpack specifically requires a standardized lifting fixture (Ref. 6.2.3, Section 33.2.4.6), it is assumed that a similar requirement will be imposed upon the STC design.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

3.2.17 **Assumption:** There will be materials accountability performed concurrently with CSNF transfer.

**Rationale:** While not specifically identified on the WHF BFDs, a material accountability will be performed. Based on operations input, an underwater video camera mounted to the fuel transfer machine will be used by an operator to view and record the serial numbers of each submerged fuel assembly and its location within a transportation cask, fuel rack, or its final TAD location. A secondary, independent check of the material inventory will be performed concurrently by quality insurance personnel who will verify the material accountability from the prerecorded video tapes.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

3.2.18 **Assumption:** DPC cutting occurs dry, within a preparation area, and with the internals flooded such that the fuel is covered with water, and is not performed underwater within the pool.

**Rationale:** A DPC cutting engineering study concluded that a partially dry approach to opening DPCs would be the most suitable method (Ref. 6.2.1, Section 2.1.1) and is captured in the BOD (Ref. 6.2.3, Section 5.2.1.3). This approach would involve performing all DPC preparation and cutting operations in a dry environment within a preparation area with the internals flooded such that the fuel is covered with water prior to breaching the DPC. Once opened, the DPC is transferred with the shield plug still in place into the pool for shield plug removal and fuel transfer. While this design change is documented in a study, it is assumed to be adopted as the design approach per the BOD. This assumption is suitable for use in this preliminary study.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

3.2.19 **Assumption:** DPC Cutting requires the removal of two lids and a shield plug.

**Rationale:** The specific designs of the DPCs vary. The *Dual Purpose Canister Opening Study* investigated the various DPC designs and documented a summary of the DPC design information (Ref. 6.2.1, Table A-2). Based on this information, the bounding case DPC utilizes an outer lid, an inner lid, and a shield plug. All three require removal prior to unloading CSNF from the DPC.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

3.2.20 **Assumption:** The DPC cutting process follows a general sequence that includes a series of basic steps required to sample, vent and open a DPC. The basic methodology for opening a DPC is listed as follows:

- |  |   |
|--|---|
| 1. Remove STC Lid  | 9. Fill DPC with water                              |
| 2. Set-up DPC cutting machine to cut DPC outer lid               | 10. Set-up DPC cutting machine to cut DPC inner lid |
| 3. Cut DPC outer lid   | 11. Cut DPC inner lid                               |
| 4. Remove DPC outer lid  | 12. Remove DPC inner lid                            |
| 5. Set-up DPC cutting machine to cut siphon and vent port covers | 13. Install DPC shield plug lifting device          |
| 6. Remove siphon and vent port covers                            | 14. Install STC lid                                 |
| 7. Connect hoses to siphon and vent ports                        | 15. Place DPC/STC into the pool                     |
| 8. Sample atmosphere inside DPC and cool, if necessary           | 16. Remove STC lid                                  |
|  | 17. Lift DPC shield plug                            |
|  | 18. Cut DPC siphon tube                             |
|  | 19. Remove DPC shield plug                          |

It should be noted that these steps are generic and in reality will vary depending on the type of DPC being cut as not all DPCs have an inner lid.

**Rationale:** This information is based on the *Dual Purpose Canister Opening Study* (Ref. 6.2.5, Section 4), which researched various DPC opening methods, including those proposed by DPC manufacturers and documented in their respective Safety Analysis Reports.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

3.2.21 **Assumption:** The process to machine off the weld areas of a typical inner and outer DPC lid is assumed to be 12 hours.

**Rationale:** The DPC lids are austenitic stainless steel (typical for SS-304L and SS-316L). The milling machine is assumed to be an end mill (Ref. 6.2.1, Section 2.3.3) utilizing a high-speed steel cutter that is a diameter of 1.0 inch with a 3-tooth, 20-degree helix angle tool profile. This milling machine is assumed to operate at a milling depth of 0.250 inches and a speed of 210 rpm. Based on the tabular data from the *Machinery's Handbook* (Ref. 6.2.37, Table 15a), the recommended feed rate is 0.003 inches per tooth and average cutting speed of 55 ft/min for high-speed steel cutters (Ref. 6.2.37, Table 13). High-speed steel cutters were chosen, rather than carbide tip tools, to be conservative as the cutting operations will be performed without any liquid cooling or lubrication. While DPCs vary in size, it is assumed the weld diameter is 70 inches in diameter. In addition, it is assumed that the weld depth that needs to be machined is 1 inch deep for the outer lid and ½ inch deep for the inner lid. To calculate the feed rate, the equation specified in the *Machinery's Handbook* (Ref. 6.2.37, p. 1041) is used:

$$f_m = f_t n_t N \quad (\text{Eq. 3})$$

Where:

$f_m$  = milling machine feed rate in inches per minute

$f_t$  = feed in inches per tooth

$n_t$  = number of teeth in the milling cutter

$N$  = spindle speed of the milling machine in revolutions per minute (rpm).  $N$  is found using the cutting speed ( $V$ ) and the tool diameter ( $D$ ):

$$N = \frac{12V}{\pi D} = \frac{12 \text{ in/ft} \cdot 55 \text{ ft/min}}{\pi \cdot 1 \text{ in}} = 210.1 \text{ rev/min} \quad (\text{Eq. 4})$$

Substituting back into the feed rate equation from above:

$$f_m = 0.003 \text{ in/tooth} \times 3 \text{ teeth} \times 210.1 \text{ rev/min} = 1.89 \text{ in/min} \quad (\text{Eq. 5})$$

To calculate the time for one pass of the cutter head:

$$\frac{\pi \times 70 \text{ in}}{1.89 \text{ in/min}} = 116.3 \text{ min} \cong 120 \text{ min} \quad (\text{Eq. 6})$$

The number of passes required is determined by the assumed cutting depth of 0.25 inches for a total depth of 1.0 inch, or four passes of the cutter head. Therefore, the total time to perform the outer lid cutting is:

$$120 \text{ min} \times 4 \text{ passes} = 480 \text{ min} = 8 \text{ hr} \quad (\text{Eq. 7})$$

Similarly, the total time to perform the 0.50 inch thick inner lid cutting of two 0.25 inch passes is:

$$120 \text{ min} \times 2 \text{ passes} = 240 \text{ min} = 4 \text{ hr} \quad (\text{Eq. 8})$$

This results in a total time of 12 hours to open the inner and outer lids of the DPCs.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

**3.2.22 Assumption:** The process to fill the TAD with borated water will take approximately 25 minutes.

**Rationale:** TAD volume is specified in the BOD (Ref. 6.2.3, Section 33.2.2.1) with a maximum outside length of 212 inches and a diameter of 66.5 inches. Ignoring the TAD wall thickness, this equates to a free volume of:

$$\frac{\pi d^2}{4} \times L = \frac{\pi (66.5 \text{ in})^2}{4} \times 212 \text{ in} = 736,324 \text{ in}^3 = 3,188 \text{ gal} \quad (\text{Eq. 9})$$

The piping, pressure, and runs are not known for this application. It can be assumed that a dedicated filling pipe could supply water at 150 gallons per minute. Thus, solving for the filling time:

$$\frac{3,188 \text{ gal}}{150 \text{ gal}/\text{min}} = 21.5 \text{ min} \cong 25 \text{ min} \quad (\text{Eq. 10})$$

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

**3.2.23 Assumption:** The process to fill the STC annulus with borated water, as specified in the WHF BFD (Ref. 6.2.22, Block 3.1.1), will take approximately 25 minutes.

**Rationale:** Similar to Assumption 3.2.22, the filling of the annulus between the STC and the TAD can be found by subtracting the TAD volume from the free volume of the STC. The flow rate in this assumption is significantly reduced as the annular space between the TAD outer diameter and the STC inner diameter is assumed small. Thus, a relatively low flow rate will be used, nominally 10 gallons per minute.

The STC dimensions are currently unknown, but are assumed to be slightly larger than the TAD dimensions. Thus, assume an STC volume of 215 inches long and a diameter of 68.5 inches. This equates to a volume of:

$$\frac{\pi d^2}{4} \times L = \frac{\pi (68.5 \text{ in})^2}{4} \times 215 \text{ in} = 492,336 \text{ in}^3 = 3,430 \text{ gal} \quad (\text{Eq. 11})$$

TAD volume is specified in the BOD (Ref. 6.2.3, Section 33.2.2.1) with a maximum outside length of 212 inches and a diameter 66.5 inches. This equates to a free volume of:

$$\frac{\pi d^2}{4} \times L = \frac{\pi(66.5 \text{ in})^2}{4} \times 212 \text{ in} = 736,324 \text{ in}^3 = 3,188 \text{ gal} \quad (\text{Eq. 12})$$

Subtracting the TAD volume from the STC and assuming a flow-rate of 10 gallons per minute provides the free volume required to be filled in a specific period of time.

$$\frac{3,430 \text{ gal} - 3,188 \text{ gal}}{10 \text{ gal}/\text{min}} = 24.2 \text{ min} \cong 25 \text{ min} \quad (\text{Eq. 13})$$

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

**3.2.24 Assumption:** TAD welding and non-destructive testing/examination require 6 hours to complete.

**Rationale:** TAD welding involves the welding of two lids with non-destructive testing/examination of each lid. The welding is assumed to be a three pass weld operating at 3 inches per minute. A setup of the weld-head is required prior to each pass requiring approximately 10 minutes, which is based on vendor provided video of a similar welding operation.

$$\frac{\pi \times 66.5 \text{ in} \times 3 \text{ passes}}{3 \text{ in}/\text{min}} = 208.9 \text{ min} \cong 210 \text{ min} = 3.5 \text{ hr} \quad (\text{Eq. 14})$$

Including the weld prep prior to each of the three weld passes, the total time is 240 minutes (4 hours) per lid.

The non-destructive testing/examination equipment and process time is currently unknown. For this study, it is assumed the non-destructive testing/examination requires 120 minutes (2 hours) to perform with a 30 minute equipment setup. The Gantt chart accounts for the additional process time for subsequent setup and tear-down of both the weld equipment and the non-destructive testing/examination equipment (See Attachment I)

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

**3.2.25 Assumption:** TAD drying is based on a vendor provided process and requires approximately 2,280 minutes (38 hours).

**Rationale:** The TAD drying process is based on the Holtec International process. Based on this vendor information, typical drying times are from 16 to 38 hours per canister, depending on the heat load of the canister and the operational practices of the site (see Appendix B). The more conservative 38 hour process is used in this study. Until definitive data is available, this assumption is suitable for use.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

- 3.2.26 **Assumption:** All incoming railcars and tractor-trailers will be chocked but not leveled or tied-down to the facility floor.

**Rationale:** Currently, operational procedures are not developed for the handling, loading, and offloading of railcars and tractor-trailers within the WHF. The naval cask handling process requires leveling and tie-down of the railcar prior to upending the naval transportation cask. However, nuclear power industry observations and benchmarking has shown that leveling and tie-down of railcars and truck-trailers is not required. The GA-9 safety analysis report (Ref. 6.2.32, pp. 7.1-1 to 7.1-2) states that the trailer could either 1) have the brakes set and the wheels chocked or 2) allow the trailer to move under the load. Observations from Sharron Harris Nuclear Power Plant applied the brakes and chocked the wheels of the railcar prior to offloading their transportation cask. Discussions with operators at Edward Hatch Nuclear Power Plant allowed the railcar to move under the load as they offloaded the Holtec HI-STAR 100 transportation casks. Per the safety analysis report, the method used is determined by the crane capability within the facility handling the cask.

The assumed operation of tying down the railcar or trailer will not be implemented, but rather simply applying the brakes and chocking the wheels. Thus this is assumed that two operators will perform this duty in 10 minutes. Until specific operational procedures are established for each transportation cask type used in the WHF, this assumption is reasonable.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

- 3.2.27 **Assumption:** All grapple and yoke change outs require 15 minutes to remove from an overhead crane and 15 minutes to install onto an overhead crane.

**Rationale:** Currently, there is not enough detailed information available to know the exact process for removing a grapple or yoke from an overhead crane. It is assumed that the process will involve removing safety bolts and sliding out a primary kingpin (See Figure 1 as an example of a typical yoke change out as performed at the Maine Yankee Nuclear Power Plant). A similar, reverse operation will be required to install the king pin and any safety bolts. Until a specific process is known, all grapple changes are assumed to require 15 minutes to disconnect and 15 minutes to reconnect.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).



Figure 1. Typical Yoke Change Out

3.2.28 **Assumption:** The process for handling a rail-based PWR or BWR bare-fuel transportation casks is assumed to be the same as for truck-based transportation casks.

**Rationale:** All rail-based transportation cask variants are assumed to be prepared for unloading and exported from the facility utilizing a similar process and timeframe as the truck-based transportation casks. This does not include the transfer of the fuel assemblies from the rail casks, which are assumed to contain 32 PWR or 68 BWR fuel assemblies each.

For example, the handling of the rail-based or truck-based transportation casks follow similar operational steps. However, the transfer of the fuel contents (i.e., the CSNF) is modeled individually and accounts for the number for the PWR or BWR fuel assemblies. It is the transportation cask preparation and handling process that is generically modeled. Until specific operational sequences, cask quantities (waste stream), and process times are established for each transportation cask type, this assumption is suitable for use in this preliminary throughput study.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

**3.2.29 Assumption:** Canister Transfer Machine movements will require 5 minutes.

**Rationale:** The distance to travel between the unloading and loading ports is slightly less than approximately 60 feet (Ref. 6.2.7). Maximum trolley speed shall be limited by design to a nominal 20 feet per minute (Ref. 6.2.4). Additionally, this operating speed of 20 feet per minute for the movement of the critical load is less than the recommended slow bridge speed of 40 feet per minute for a 300 to 499 ton load per NOG-1 (Ref 6.2.1, Table 5332.1-1). While the assembly weight of the canister transfer machine is 500 tons (Ref. 6.2.37), where the crane load, a loaded TAD canister (Ref. 6.2.3, Section 33.2.2.2) and the trolley shield bell assembly is assumed to be approximately 200 tons, depending on the shielding materials

Also, it is assumed that the CTM will require 30 seconds to accelerate and 30 seconds to decelerate from the operating speed of 20 feet per minute. The distance traveled by the bridge during its acceleration and deceleration can be found as:

$$\frac{1}{2} a \cdot t^2 = \frac{1}{2} \left( 40 \frac{\text{ft}}{\text{min}^2} \right) (0.5 \text{ min})^2 = 5 \text{ ft} \quad (\text{Eq. 15})$$

The total distance required to travel at the full operating speed of 20 feet per minute is:

$$60 \text{ ft} - (2 \times 5 \text{ ft}) = 50 \text{ ft} \quad (\text{Eq. 16})$$

The time required to travel the 50 feet at 20 feet per minute is 2.5 minutes. Adding the acceleration and deceleration time to the travel time, a total of 3.5 minute is required. After the load has stopped, minor swinging-oscillations of the canister load will occur. It is assumed that one minute is required for the natural dampening of these oscillations. Therefore, the total time required is 4.5 minutes. This value is simply rounded to 5 minutes for the CTM movement.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

**3.2.30 Assumption:** Transportation cask cooling is not accounted for in the throughput estimates.

**Rationale:** Transportation casks contents may be too thermally hot to allow for the introduction of borated water as part of the cask preparation and unloading activities. Cask cooling may be required, however, the method for cask cooling is undefined and subsequent process times can not be estimated. In addition, the frequency for cask cooling can not be quantified without a better understanding of the waste stream thermal properties and criteria for cask cooling. Until further definition of cask cooling is developed, transportation cask cooling is not accounted for in the throughput estimates and may degrade the performance of the facility.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

**3.2.31 Assumption:** Shield doors used in the WHF take 5 minutes to open and close.

**Rationale:** Some shield doors in the WHF weigh upwards of 300 tons with a travel of approximately 20 feet (Ref. 6.2.6). The mass of these doors limits the speed in which these doors can move. Engineering judgment has been used to determine the 5 minute time frame. This time can be considered reasonable for the preliminary analysis.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

3.2.32 **Assumption:** Manpower will be sufficient to support all operational phases based on the WHF operating on the operational work week schedule. This assumption includes sufficient personnel to support activities required to be performed concurrently identified in this throughput.

**Rationale:** When a facility is designed, startup, operation, and maintenance personnel to support these functions are factored into the design once the operation and maintenance schedule has been identified for a facility.

**Used in:** This assumption was used in the development of the throughput model (Attachment I) and in the WHF Gantt chart (Appendix A).

### 3.3 Methodology

The preliminary throughput estimate was generated based on the WHF BFDs<sup>5</sup> and general arrangement drawings<sup>6</sup>. The diagrams were used to formulate the high-level sequence of events for the receipt, unloading, and packaging of waste forms. Once the high-level processes and logic were captured in the WHF Gantt charts, a detailed process was defined for each high-level process step (See WHF Gantt charts in Attachment I and as summarized in Appendix A). The detailed WHF processes were represented as discrete process steps, where process times were estimated (Assumption 3.2.9) and step-wise logic formulated. The discrete processes were also assigned appropriate resources, such as cranes, the canister transfer machine, drying equipment, DPC cutting equipment, SFTM, weld stations, etc.

Once the detailed process steps and subsequent logic were captured in the Gantt chart, then the processes, times, and logic were represented in a process modeler. The process modeling software (SimCAD™ Pro) is a deterministic, discrete, and local simulation tool that is more robust than a Gantt chart, especially in modeling complex, logic-driven systems. This discrete process modeler does not rely on a mathematical model with an underlying equation. Although the model is represented formally, individual objects and resources in the model are represented directly (rather than by their density, concentration, or formula). Each model process and resource possesses an internal state and conforms to a set of behaviors or rules. The specified process determines how the object is updated from one time-step to the next within the model environment.

### 3.4 Use of Computer Software

Software tools used to develop this non-quality affecting engineering study are applied in scoping determinations and used to assess the feasibility of the Nuclear Facility in meeting throughput requirements; and therefore, are classified as Level 2 usage and are not required to be qualified per IT-PRO-0011, *Software Management* (Ref. 6.1.2, Attachment 12).

The process simulation software used for this throughput model is SimCAD™ Pro 8.0 Build-1371. Standard functions of SimCAD™ Pro were used to model the WHF processes. The SimCAD™ Pro files are contained on a compact disc (Attachment I).

Standard functions of Microsoft Excel™ for Windows, Version 2003 SP3 (Build 11.8169.8172), were used in this study to display results in a tabular form and as inputs to the SimCAD™ Pro model. The Microsoft Excel™ files are contained on a compact disc (Attachment I).

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<sup>5</sup> Block flow diagrams include Revision 00A of the Level 2 and Draft Revision 00Bb of the Level 3 diagrams (Refs. 6.2.11, 6.2.12, 6.2.13, 6.2.14, 6.2.15, 6.2.16, 6.2.17, 6.2.18, 6.2.19, 6.2.20, 6.2.21, 6.2.22, 6.2.23, 6.2.24, 6.2.25, 6.2.26, 6.2.27, and 6.2.28)

<sup>6</sup> Site layout drawing include Revision 000 for the first and second floor and one elevation (Refs. 6.2.6, 6.2.7 6.2.8, 6.2.9 and 6.2.10)

Standard functions of Microsoft Office Project™ Professional 2003 SP3 (Build 11.3.2007.1529.15), was used in this study to determine the waste form processing times and for validating the SimCAD™ Pro model. The Microsoft Project™ files are contained on a compact disc (Attachment I) and are summarized in Appendix A.

#### 4.0 DESCRIPTION OF ALTERNATIVES CONSIDERED

This preliminary throughput study investigated a single preliminary facility layout, as documented in the WHF BFDs and general arrangement drawings. However, twelve different waste streams were analyzed, as shown in Table 3 and further described in Section 4.1. The waste streams were created to saturate the WHF throughput model; and thereby, estimating maximum throughput for the particular waste stream (Assumptions 3.2.1 and 3.2.2). This maximum throughput is considered optimum, as any external or process delays will degrade the throughput from this optimum.

Table 3 shows the composition of each waste stream case by quantity of transportation casks per type. While some waste streams were arbitrarily selected, most were selected to test the sensitivity of the WHF's throughput to changes in waste stream.

Table 3. Waste Streams Cases by Transportation Cask Type

Waste Stream Type	Waste Stream Case – Transportation Cask											
	1	2	3	4	5	6	7	8	9	10	11	12
	Avg	Peak	DPC Only	DPC Only	Truck Only	Truck Only	Mix	Mix	Mix	Sm. Rail	Med. Rail	Lg. Rail
Truck PWR	72	145	-	-	152	130	140	100	60	-	-	-
Truck BWR	23	55	-	-	48	70	44	22	14	-	-	-
Rail PWR DPC	12	27	160	118	-	-	11	62	100	-	-	-
Rail PWR HI-STAR	1	2	16	12	-	-	1	6	10			
Rail BWR DPC	2	9	23	67	-	-	4	10	16	-	-	-
Rail BWR HI-STAR	-	-	1	3	-	-	-	-	-			
Rail PWR	-	-	-	-	-	-	-	-	-	154	154	154
Rail BWR	-	-	-	-	-	-	-	-	-	83	83	83
Total	110	238	200	200	200	200	200	200	200	237	237	237

#### 4.1 Waste Stream Cases

For each waste stream case shown in Table 3, the specific delivery rate to the repository is a uniform distribution. Using Case 5 as an example, if there were 152 PWR truck casks allocated to be delivered within the waste stream case, then the delivery would be uniformly spread across 75 percent of the year (Assumption 3.2.3).

$$\frac{(365 \text{ days} \times 24 \text{ hr/day} \times 60 \text{ min/hr}) \times 75\%}{152 \text{ casks}} = \frac{394,200 \text{ min}}{152 \text{ casks}} = 2,593 \text{ min/cask} \quad (\text{Eq. 17})$$

Thus, there would be a PWR truck cask arriving every 2,593 minutes, or 43.2 hours. This receipt methodology is applied to each of the transportation cask types for the particular waste stream. By following the same formula as above for the waste stream Case 1 (Table 3), there will be a total of 72 PWR truck casks each arriving every 91 hours, 23 BWR truck cask each arriving every 286 hours, 13 PWR DPC rail casks (HI-STAR and generic) each arriving every 505 hours, and a

2 BWR DPC rail casks each arriving every 3,285 hours. This delivery methodology for the repository is applied to all waste stream cases.

#### **4.1.1. Case 1 and 2 – 2002 Waste Stream Case**

The waste stream for Cases 1 and 2 are based on the data provided in the *2002 Waste Stream Projections Report* (Ref. 6.2.29). The waste stream used has been out of the reactor a minimum of 10 years and the youngest fuel is delivered first, referred to as the 10-YFF case. The data from this case was analyzed to estimate a likely delivery to the WHF. The 10-YFF case data<sup>7</sup> was analyzed by using a pivot table to extract the total number of cask deliveries by type and by year of delivery. From this data, two cases were determined, an average and a peak—Cases 1 and 2, respectively. The average case simply takes the average number of PWR and BWR transportation casks to be delivered over the entire delivery period. The peak extracts the years where the number of transportation casks deliveries are the greatest. For example, the peak case shows that 145 PWR truck casks are to be delivered in year 5 and that 55 BWR truck casks are to be delivered in year 6. Thus, the peak case (Case 2) extracts the maximum delivery regardless of the year of delivery. For Case 1, the percentage split of transportation casks delivered to the repository is 77 percent PWR and 23 percent BWR. For Case 2, the percentage split is 73 percent PWR and 27 percent BWR.

#### **4.1.2. Case 3 – PWR/BWR Split for DPC**

Case 3 is a DPC only case where the total number of DPCs delivered is arbitrarily set at 200. This is significantly more DPCs than expected within a year, but as discussed above was purposely set high to saturate the WHF throughput model; and thereby, estimate the maximum throughput for the particular waste stream (Assumptions 3.2.1 and 3.2.2).

The split between PWR and BWR DPCs was determined by examining the 10-YFF case data, as discussed in Case 1-2 above. In addition, the percentage split for HI-STAR DPCs for both PWR and BWR waste streams was determined. For the entire delivery schedule, 88 percent of the DPCs to be delivered are PWR and 12 percent are BWR. Assuming 200 DPCs to be delivered in a particular year equates to 176 PWR and 24 BWR DPCs. Of the 176 PWR DPCs, 16 are HI-STAR PWR DPCs resulting in 160 standard DPCs. Thus, for PWR DPCs, approximately nine percent are HI-STAR PWR DPCs. And, of the 24 BWR DPCs, 1 is a HI-STAR BWR DPC resulting in 23 standard DPCs. Again, for BWR DPCs, approximately four percent are HI-STAR BWR DPCs.

#### **4.1.3. Case 4 – Arbitrary PWR/BWR Split for DPC**

Like Case 3 above, Case 4 is a DPC only case where the total number of DPCs delivered is set at 200 to saturate the model. The split between PWR and BWR was slightly modified to 65 percent PWR and 35 percent BWR to help identify any sensitivity to fuel type within a waste stream and its effects on total throughput. A similar percentage of standard and HI-STAR DPCs is made.

#### **4.1.4. Case 5 – PWR/BWR Split of Truck Transportation Casks**

Case 5 is a truck cask only case where the total number of truck casks delivered is once again arbitrarily set at 200. Like the previous cases, this is significantly more truck casks than expected within a year, but as discussed above was purposely set high to saturate the WHF throughput model; and thereby, estimating maximum throughput for the particular waste stream (Assumptions 3.2.1 and 3.2.2).

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<sup>7</sup> See Attachment I, Excel File "Waste Stream Evaluation", Tab "B\_YFF10-Casks"

The split between PWR and BWR truck casks was determined by examining the 10-YFF case data, as discussed in Case 1-2 above. For the entire delivery schedule, 76 percent of the truck casks to be delivered are PWR and 24 percent are BWR. Assuming 200 truck casks to be delivered in a particular year equates to 152 PWR and 48 BWR DPCs.

#### **4.1.5. Case 6 – Arbitrary PWR/BWR Split of Truck Transportation Casks**

Like Case 5 above, Case 6 is a truck cask only case where the total number of truck casks delivered is set at 200 to saturate the model. The split between PWR and BWR was slightly modified to 65 percent PWR and 35 percent BWR to help identify any sensitivity to fuel type within a waste stream and its effects on total throughput.

#### **4.1.6. Cases 7 through 9 – Truck and DPC Sensitivity Studies**

Cases 3-4 and 5-6 show the boundaries of the waste streams to help identify sensitivities in the throughput to changes in the waste stream. While Cases 3-4 were DPC only and Cases 5-6 were truck cask only, Cases 7 through 9 were set up to vary the mix of DPCs and truck casks from one extreme to the other. Waste stream Case 7 starts with a heavy proportion of truck casks and a light proportion of DPCs. Case 8 blends the number of truck casks and DPCs. Case 9 has a heavy proportion of DPC and a light proportion of truck casks.

#### **4.1.7. Cases 9 through 12 – Small, Medium, and Large Bare Fuel Rail Casks**

Cases 9 through 12 were developed specifically to determine the effects on throughput by using bare-fuel transportation casks that contained more fuel assemblies per cask than a standard truck cask, which is a more efficient mode of operation as it requires less cask handling per TAD. Based on input from the Total System Model group, these rail cask sizes are the same size casks used in their respective throughput cases. The three cases are the small, medium and large casks that contain 8/20, 18/42, and 32/68 PWR/BWR fuel assemblies per cask, respectively.

## **4.2 Operations Concept**

As discussed in Assumption 3.2.6, the concept of operations for the WHF has been modified for this throughput study to represent a round-robin scheduling methodology. The operations are assumed to be a step-wise, sequential process where objects (transportation casks, STCs, DPCs, etc.) will move from station to station. And, once a station becomes available another item will move into that station. This process allows for multiple truck casks, DPCs, and TADs to be processed simultaneously, significantly improving the parallel operations within the facility.

The process flow for these three items (truck casks, DPCs, and TADs)<sup>8</sup> is each shown separately in Figure 2. In general, this process flows circularly from the conveyance on the east side of the building, to the north side of the building for preparation operations, to the pool on the west for loading/unloading operations, to the southern side for exit and welding operations, and back to the conveyance on the east side.

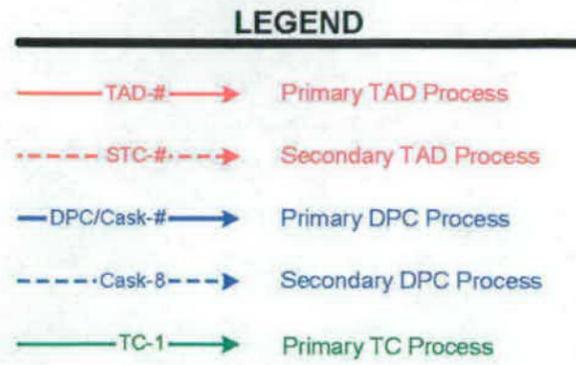
While any order or number of objects can be processed, a summary-level example of how this circulatory flow works with the round-robin scheduling can be described with a couple of truck-based transportation casks, a couple of TADs, followed by a couple of DPCs.

1. A truck cask arrives on its conveyance in the east side of the pool room.
2. The truck cask is moved from its conveyance to preparation station #1 (operation TC-1 shown on Figure 2) and the conveyance is moved out of the facility.

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<sup>8</sup> For bounding purposes, a secondary rail-based waste stream is investigated in this throughput study but is not considered a primary waste stream and subsequently its operational flow is not shown in Figure 2.

3. A second truck cask is moved into the facility on its conveyance.
4. Once prepared for unloading, the first truck cask is moved to the pool (TC-2). Once in the pool and the overhead crane is free, the second truck cask is moved into the preparation station (TC-1). There are now two truck casks within the facility, one in the pool being unloaded and one in the preparation station #1. The conveyance for the second truck cask is moved out of the facility while truck cask 1 is being unloaded and truck cask 2 is being prepared.
5. The next incoming object is an empty TAD within an STC (Assumption 3.2.13). As the conveyance brings in the STC/TAD, the unloaded truck cask 1 is moved from the pool to preparation station #2 (TC-3), truck cask 2 is moved from preparation station #1 to the pool (TC-2), and then the incoming STC/TAD is moved from its conveyance to preparation station #1 (TAD/STC-1). At this point in time, there are three simultaneous operations occurring—one in preparation station #1, one in the pool, and one in preparation station #2.
6. In order for the round-robin process to continue, the truck cask in preparation station #2 must be moved to its conveyance (TC-4) and removed from the facility. This will open preparation station #2 for the next operation, which is moving truck cask 2 out of the pool and into preparation station #2 (TC-3). This in turn, opens up the pool so that the TAD/STC 1 can be moved from preparation station #1 to the pool (TAD/STC-2).
7. While truck cask 2 and TAD/STC-1 is being moved and truck cask 1 is now out of the facility, the second STC/TAD is brought into the facility and moved to preparation station #1 (TAD/STC-1). Once again, there are three simultaneous operations occurring—TAD/STC 2 in preparation station #1, TAD/STC 1 in the pool being loaded, and truck cask 2 in preparation station #2.
8. Truck cask 2 is moved from preparation station #2 to its conveyance, which was brought into the facility. Once the truck cask is moved out of the facility, the DPC is moved into the facility within a rail-transportation cask (RC) on a railcar. Meanwhile, TAD/STC 1 is moved from the pool to the TAD closure station (TAD/STC-3), which opens up the pool to move TAD/STC 2 from the preparation station to the pool (TAD/STC-2).
9. Then, DPC 1 is moved from the conveyance to the preparation station #1 (DPC/RC-1).
  - a. The DPC requires transfer from its rail-based transportation cask to a DPC-STC for in-facility handling. Once prepared, the DPC and its rail-based transportation cask is moved into the cask transfer room (DPC/RC-2) where the rail-based transportation cask lid is removed and the DPC is pulled up into the bell of the canister transfer machine. The rail-based transportation cask lid is placed back onto the cask, and the empty cask is moved back to the preparation station #1 (RC-3).
  - b. The transportation cask is then prepared for exit and moved back to its railcar (RC-4).
  - c. Once the railcar with the empty rail-based transportation cask is removed from the facility, a STC is brought into the facility and is moved to preparation station #1 (STC-5) and prepared for DPC loading.
  - d. The STC is moved into the cask unloading room under the cask transfer port (STC-6). The lid of the STC is removed and the DPC is loaded into the STC. The lid is replaced on the STC and the DPC/STC is moved back to preparation station #1 (DPC/STC-7).
  - e. At this point the DPC/STC is ready for cutting and is moved from preparation station #1 to the DPC cutting station (DPC/STC-8).



**ACRONYMS**

AO	Aging Overpack
DPC	Dual-Purpose Canister
RC	Rail Cask
STC	Shielded Transfer Cask
TAD	Transport, Aging, and Disposal Truck Cask
TC	

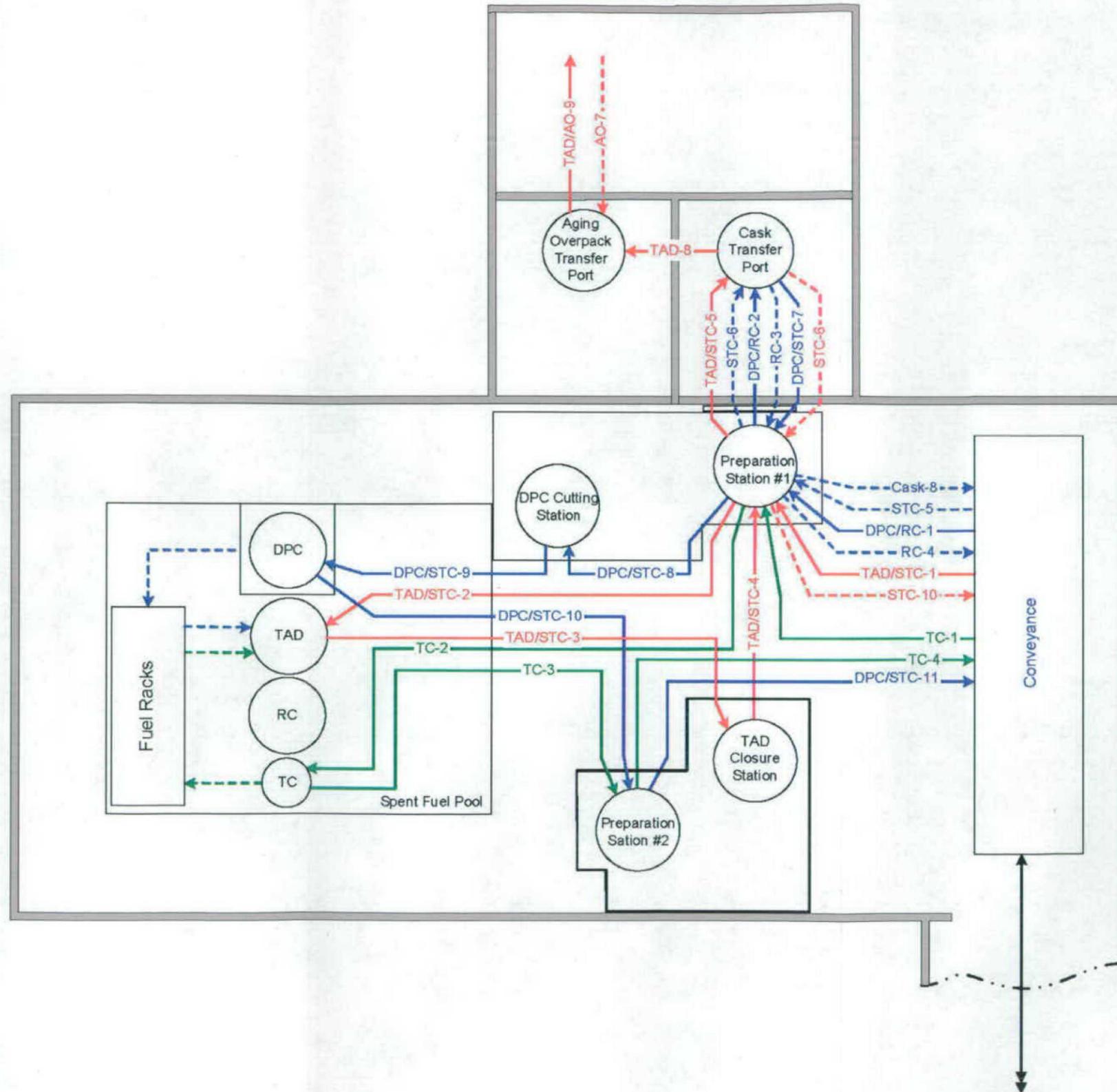


Figure 2. Summary WHF Process Flow

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10. The preparation station #1 is now available; and in this example, a second DPC is in the queue for processing within the facility. However, the preparation station #1 must not become occupied as TAD/STC 1 is nearing completion of the welding operations. Rather than allowing DPC 2 to enter the facility, the TAD/STC 1 is allowed to complete its welding operation and preparation station #1 remains idle.
11. Once complete with welding, the TAD/STC 1 is transferred from the TAD closure station to preparation station #1 (TAD/STC-4). At this point, the TAD must be transferred out of the STC and placed into an aging overpack for transfer to either the Aging Facility or to the Canister Receipt and Closure Facility.
  - a. The TAD/STC 1 is moved under the cask transfer port of the cask transfer room (TAD/STC-5).
  - b. The lid of the STC is removed and the lid of an awaiting aging overpack (AO-7) is removed and staged within the canister transfer room.
  - c. The TAD is raised into the bell of the canister transfer machine. The CTM slews over to the aging overpack transfer port and lowers the TAD into the aging overpack (TAD-8).
  - d. Once the TAD is in the aging overpack, the CTM retrieves the aging overpack lid and places the lid onto the aging overpack, and then the aging overpack is moved out of the facility (TAD/AO-9).
  - e. Once the lid is on the aging overpack, the STC lid is retrieved and placed back onto the now-empty STC, simultaneously with the aging overpack being moved out.
  - f. The empty STC is moved to the preparation station #1 (STC-6).
12. Once prepped for exit, the empty STC is then moved to the conveyance (STC-10), which frees up preparation station #1. At this point in time, 1) there is TAD/STC-2 in the TAD closure station, 2) DPC/STC 1 in the DPC cutting station, and 3) DPC/RC 2 in the queue to enter the facility. Both the pool and the preparation station #1 are idle.
13. Once complete with cutting operations, DPC/STC 1 is moved into the pool for unloading operations (DPC/STC-9). Now both the preparation station #1 and the DPC cutting station is idle.
14. With TAD/STC 2 finishing welding and DPC/RC 2 in the entrance queue, the model must make the decision of which object to place into preparation station #1. TADs have been set as the priority for the model, as processing TADs has a direct affect on MTHM processed and number of TADs created. Therefore, DPC/RC 2 is still forced to wait as TAD/STC 2 finishes welding and preparation station #1 remains idle.
15. While waiting for welding to finish, DPC/STC 1 is able to move from the pool to preparation station #2 (DPC/STC-10).
16. Once complete, the TAD/STC 2 is moved from the TAD closure station to preparation station #1 and follows the same process as described in step 11, above.
17. After the TAD is loaded into an aging overpack and the empty TAD-STC exits the facility, the DPC/RC 2 waiting in the queue is permitted to enter the facility for processing.

This round-robin process continues to receive and process truck casks, DPCs, and TADs in a continuous, circular operation maximizing the use of the preparation, cutting, and welding stations.

## 5.0 EVALUATION OF ALTERNATIVES

### 5.1 Throughput Results

This WHF throughput model processed the maximum possible transportation casks and DPCs (based on the waste stream case) per year, which results in the maximum theoretical throughput. The throughput results are presented in total number of TADs exported from the facility (Table 4), the estimated MTHM for those TADs (Table 5), and the number of transportation casks received for processing within the WHF (Table 6).

As expected, the total number of TADs produced per year varied by the type and makeup of input waste stream. The truck-only waste streams produced significantly less TADs per year at 36. The DPC-only waste stream produced 46-47 TADs per year. The rail, bare-fuel only waste stream produced the theoretical maximum throughput at 54-74 TADs per year.

Table 4. Throughput in Terms of TADs Produced

Waste Stream Type	Waste Stream Case											
	1	2	3	4	5	6	7	8	9	10	11	12
	Avg	Peak	DPC Only	DPC Only	Truck Only	Truck Only	Mix	Mix	Mix	Sm. Rail	Med. Rail	Lg. Rail
PWR	34	33	40	40	27	23	35	46	47	33	45	42
BWR	13	7	7	6	9	13	7	6	5	21	26	32
Total	47	40	47	46	36	36	42	52	52	54	71	74

Source: Attachment I, Excel File "Summary-output.xls", Tab "Results"

Based on the number of TADs produced per year, an estimate for the annual MTHM can be determined by multiplying the respective TAD capacity by the MTHM per fuel assembly. As discussed in Assumption 3.2.10, the average MTHM per PWR and BWR fuel assembly is 0.433 and 0.174, respectively.

$$MTHM_{PWR} = 21^{Assy/TAD} \times 0.433^{MTHM/Assy} = 9.093^{MTHM/TAD} \quad (Eq. 18)$$

-OR-

$$MTHM_{BWR} = 44^{Assy/TAD} \times 0.174^{MTHM/Assy} = 7.656^{MTHM/TAD} \quad (Eq. 19)$$

To provide an estimate for throughput in terms of MTHM per year, the TAD quantities from Table 4 are multiplied by the MTHM per TAD resulting in the values in Table 5.

Table 5. Throughput in Terms of MTHM for Commercial SNF

Waste Stream Type	Waste Stream Case											
	1	2	3	4	5	6	7	8	9	10	11	12
	Avg.	Peak	DPC Only	DPC Only	Truck Only	Truck Only	Mix	Mix	Mix	Sm. Rail	Med. Rail	Lg. Rail
PWR	309	300	364	364	246	209	309	418	427	300	409	382
BWR	100	54	54	46	69	100	54	46	38	161	199	245
Total	409	354	418	410	315	309	363	464	445	461	608	627

Note: Average MTHM per assembly is based on Assumption 3.2.10.

As shown in Table 5, the 307 MTHM per year requirement (Criterion 3.1.1) was met for all cases, where the 307 MTHM is combined from 230 MTHM per year of bare CSNF from legal weight trucks, over-weight trucks and rail based bare fuel casks, and 77 MTHM per year of CSNF in DPCs by rail.

The throughput in terms of the transportation casks received is presented in Table 6, below.

Table 6. Throughput in Terms of Transportation Casks Processed

Waste Stream Type	Waste Stream Case											
	1	2	3	4	5	6	7	8	9	10	11	12
	Avg.	Peak	DPC Only	DPC Only	Truck Only	Truck Only	Mix	Mix	Mix	Sm. Rail	Med. Rail	Lg. Rail
Truck PWR	71	73	-	-	145	124	106	38	18	-	-	-
Truck BWR	27	23	-	-	47	67	27	9	6	-	-	-
Rail PWR DPC	14	12	34	26	-	-	9	25	30	-	-	-
Rail PWR HI-STAR DPC	1	1	5	16	-	-	4	4	4	-	-	-
Rail BWR DPC	5	2	4	3	-	-	1	3	3	-	-	-
Rail BWR HI-STAR DPC	-	-	1	1	-	-	-	-	-	-	-	-
Rail PWR	-	-	-	-	-	-	-	-	-	90	55	37
Rail BWR	-	-	-	-	-	-	-	-	-	48	29	23
Total	118	111	44	46	192	191	147	79	61	138	84	60

Source: Attachment I, Excel File "Summary-output.xls", Tab "Results"

The throughput simulation model continues to process right up to the end of the year (see Assumption 3.2.3). Any transportation casks being prepared for processing are counted as a cask received, but there may not have been enough time to fully process and unload the cask contents at the end of the year's time. Also, fuel assemblies reside in the pool racks at the end of the year, and subsequently are not accounted for in the MTHM calculations as they are not processed into TADs.

## 5.2 Resource Utilization and Optimization

A primary purpose for performing throughput analyses is to understand which processes and systems impede the flow of materials through the facility. When investigating throughput, a rule of thumb is used to determine if any one resource is saturated; that is, the rule of thumb is used to determine if a crane, trolley, weld cell, or any other arbitrary resource is being over-utilized and thereby impeding throughput. Typically, a process becomes saturated between 65 and 85 percent utilization. Table 7 shows the resource utilization for the primary cranes, canister transfer machines, and weld cells.

A first review of the utilization results shows that no single resource is overloaded. This indicates that no single piece of equipment is over utilized. Therefore, some other factor is impeding the flow of materials through the facility rather than a single resource. Three items are discussed below, Crane Utilization, the use of Preparation Station #1, and bare-fuel rail casks.

Table 7. Percent Utilization of Primary Equipment

Equipment or Resource	Waste Stream Case (%)											
	1	2	3	4	5	6	7	8	9	10	11	12
	Avg.	Peak	DPC Only	DPC Only	Truck Only	Truck Only	Mix	Mix	Mix	Sm. Rail	Med. Rail	Lg. Rail
Auxiliary Pool Crane	9.61	8.84	4.30	4.34	14.29	14.37	11.35	6.99	5.56	11.5	8.52	6.99
CTM Maintenance Crane	0.69	0.52	1.52	1.54	-	-	0.49	1.07	1.27	-	-	0.00
Canister Transfer Machine	16.07	12.08	35.54	35.33	0.84	0.85	11.60	24.31	28.37	1.31	1.65	1.74
Cask Handling Crane	24.88	22.87	14.15	14.52	34.32	35.13	28.81	19.94	16.76	29.35	23.84	21.44
Cask Prep Area	14.93	13.05	13.73	14.2	15.34	15.55	15.39	14.81	14.26	14.42	13.20	12.10
Cask Transfer Trolley	17.22	13.88	27.41	27.74	7.34	7.40	14.19	22.57	24.84	8.88	10.18	10.22
DPC Cutting Jib Crane	4.86	3.65	10.63	10.71	-	-	3.16	7.54	8.71	-	-	0.00
DPC Cutting Machine	7.24	5.43	15.82	15.91	-	-	4.72	11.21	13	-	-	0.00
DPC Cutting Station	9.08	6.80	19.83	19.98	-	-	5.93	14.06	16.28	-	-	0.00
Entrance Vestibule Crane	8.70	8.06	3.50	3.27	13.51	13.62	10.53	5.94	4.61	9.91	5.97	4.34
Mobile Access Platform	15.88	14.64	6.98	7.26	24.08	24.32	19.14	11.36	9.00	18.48	12.26	9.53
NDE Equipment	11.39	9.69	11.46	11.46	8.85	8.87	10.17	12.60	12.60	13.02	17.19	17.61
Pool Area	32.85	29.03	24.87	24.49	38.17	39.39	34.41	29.06	26.40	37.97	36.66	35.94
Prep Station #1	30.10	26.06	30.52	31.13	29.90	29.99	30.80	30.21	29.72	25.71	20.83	18.15
Prep Station #1 Jib Crane	10.39	8.39	17.22	17.49	4.38	4.36	8.55	13.72	15.06	5.31	6.13	6.09
Prep Station #2	4.69	4.36	2.93	3.02	6.64	6.77	5.48	3.74	3.26	4.86	2.97	2.10
Prep Station #2 Jib Crane	0.53	0.41	1.15	1.20	-	-	0.36	0.86	0.98	-	-	0.00
SFTM	9.54	7.70	9.92	9.60	7.21	7.74	8.01	9.76	9.72	11.77	15.61	17.08
TAD Canister Welding Machine	18.11	15.40	18.26	18.23	14.08	14.11	16.19	20.02	20.03	20.70	27.33	28.01
TAD Closure Jib Crane	20.03	17.02	20.00	19.96	15.71	15.73	17.89	22.15	22.17	23.1	30.5	31.23
TAD Closure Station	20.00	17.02	20.15	20.12	15.55	15.60	17.89	22.12	22.15	22.92	30.17	30.94
Transportation Cask Vestibule (Entrance Vestibule)	19.1	17.59	8.97	9.11	28.48	28.65	22.92	13.78	11.20	21.51	13.9	10.62

Source: Attachment I, Excel File "Results.xls"

5.2.1. Preparation Station Review

Preparation station #1 has been allocated multitude of tasks. Primarily, this station prepares the incoming truck transportation casks, rail-based DPC transportation casks, and new TADs. Also, this preparation station assists in the transfer of DPCs from their respective transportation cask into its STC for further processing within the WHF. As introduced in Assumption 3.2.6 and further described in the concept of operations (Section 4.2), the WHF general process flows circularly from the conveyance on the east side of the building, to the north side of the building for

preparation operations, to the pool on the west for loading/unloading operations, to the southern side for exit and welding operations, and back to the conveyance on the east side.

However, this circular process flow is interrupted by a loaded and welded TAD, as is shown in Figure 2. The current concept of operations for the WHF is that all TADs exit the facility within aging overpacks. Aging overpacks are loaded by the canister transfer machine, located north of preparation station #1. Once welding operations are complete, the loaded and welded TAD is transferred within its STC back to preparation station #1. Preparation station #1 must be available to the TAD, otherwise the facility would become blocked and not be able to further process—essentially locking up the facility. Therefore, the preparation station is not allowed to accept any incoming objects when the TAD closure operations are approximately 50 percent complete. This ensures that the preparation station is available to the loaded and welded TAD. The consequence is that the preparation station remains idle for long periods of time, as is shown by the low utilizations in Table 7, above

The requirement for TADs to exit the facility within aging overpacks should be reviewed as it requires the material flow through the facility to crisscross. Alternatively, improved process flow should be evaluated to reduce or eliminate otherwise conflicting process flows.

### **5.2.2. Crane Utilization Review**

Reviewing the facility layout drawings (Refs. 6.2.6, 6.2.7 and 6.2.8) and the concept of operation (Section 4.2 and Figure 2), overhead cranes are the primary conveyance through the WHF. The three primary cranes are the cask handling crane, the auxiliary pool crane, and the entrance vestibule crane. The cask handling crane and the auxiliary crane have operating envelopes that span the entire cask preparation area (including the pool area) and a portion of the transportation cask vestibule. The cask preparation area is divided into two zones—the pool area and the preparation area. The entrance vestibule crane spans both the transportation cask vestibule and the preparation area of the cask preparation area. In addition, there is a SFTM that operates exclusively over the pool area.

To avoid interference between the cranes or SFTM, only one crane or SFTM is allowed to operate at a time within a particular zone, which is either within the pool area, the preparation area, or the entrance vestibule area. Because the auxiliary pool crane operates on the same crane rail as the cask handling crane, neither crane can pass by the other. No two loaded cranes can occupy or pass through the same zone as another crane.

Simply, one crane has to wait for the other to complete its job prior to operating. This inability to move across zones and pass-by each other significantly restricts the crane movements, which is the primary conveyance through the WHF. These restrictions are apparent in the overall low utilizations shown in Table 7 as each piece of equipment is waiting on another to complete its job so that it can operate. Thus, the low throughput in the WHF can be primarily attributed to the crane and facility layout as well as the poor material flow planning.

### **5.2.3. Bare-Fuel Rail Cask Review**

Similar to DPC operations, rail-based bare-fuel transportation casks contain more fuel per cask than a similar truck cask. As discussed in Section 4.1.7, three different bare-fuel rail casks were used as input to the model—small casks containing either 8 PWR or 20 BWR fuel assemblies, a medium cask containing either 18 PWR or 42 BWR, and a large casks containing 32 PWR or 68 BWR fuel assemblies per cask, respectively. The cask handling operations were performed using the same process as the truck casks, but due to their increased capacity require less transportation casks to fill a TAD. Therefore, for these cases the primary bottleneck is TAD closure and the respective exit through preparation station #1. The higher utilizations in the SFTM and TAD closure station reflect this (Table 7).

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### **6.3 Design Constraints**

None

### **6.4 Design Outputs**

This engineering study will be utilized by management to assess the adequacy of the WHF design in meeting throughput expectations and/or requirements. This study may also be used to support bounding assumptions for transportation cask quantities, TAD quantities, and various other throughput related assumptions.

## **7.0 APPENDICES**

**APPENDIX A -  
WHF SUMMARY GANTT CHART**

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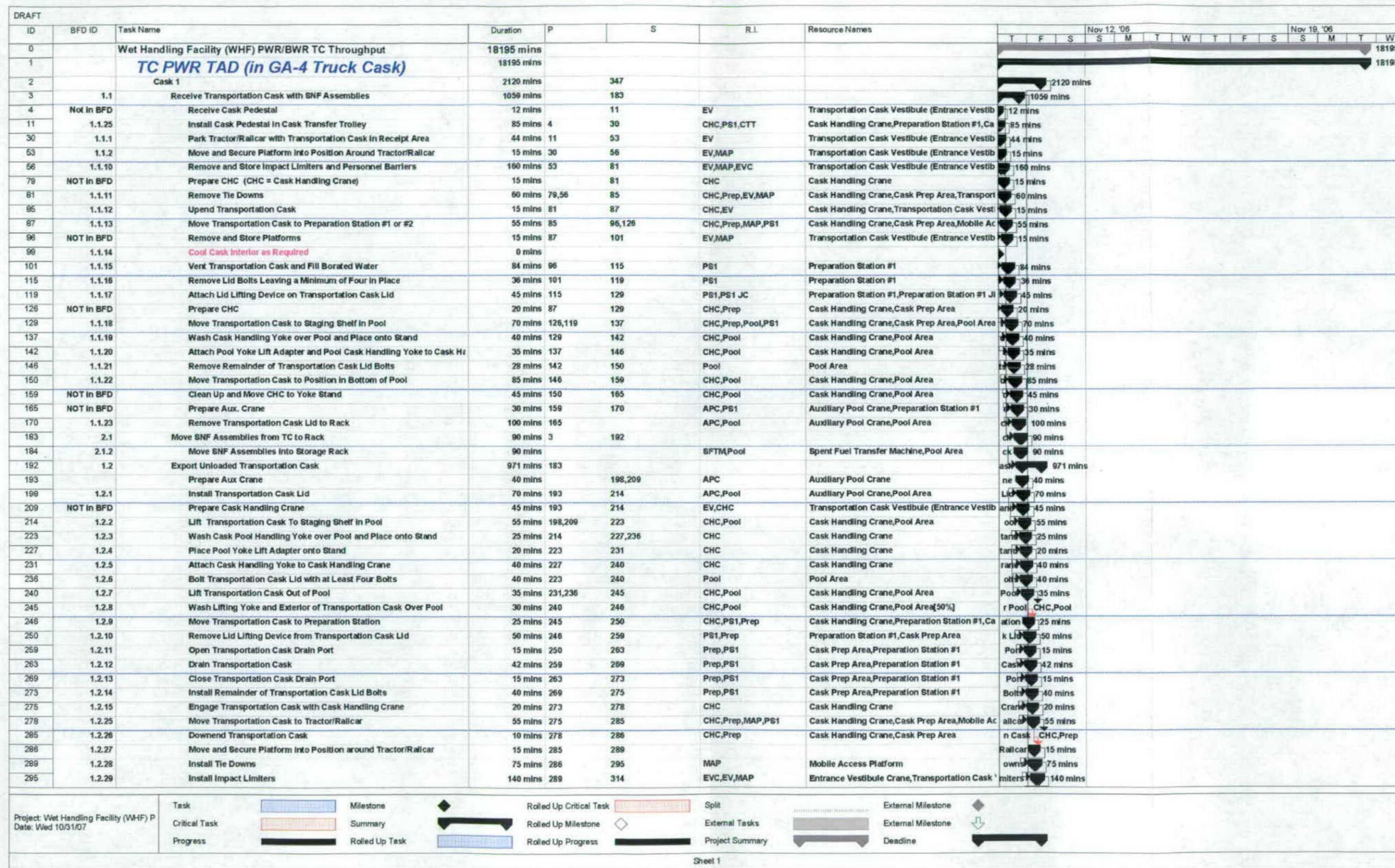


Figure A-1. Summary WHF Gantt Chart – Sheet 1

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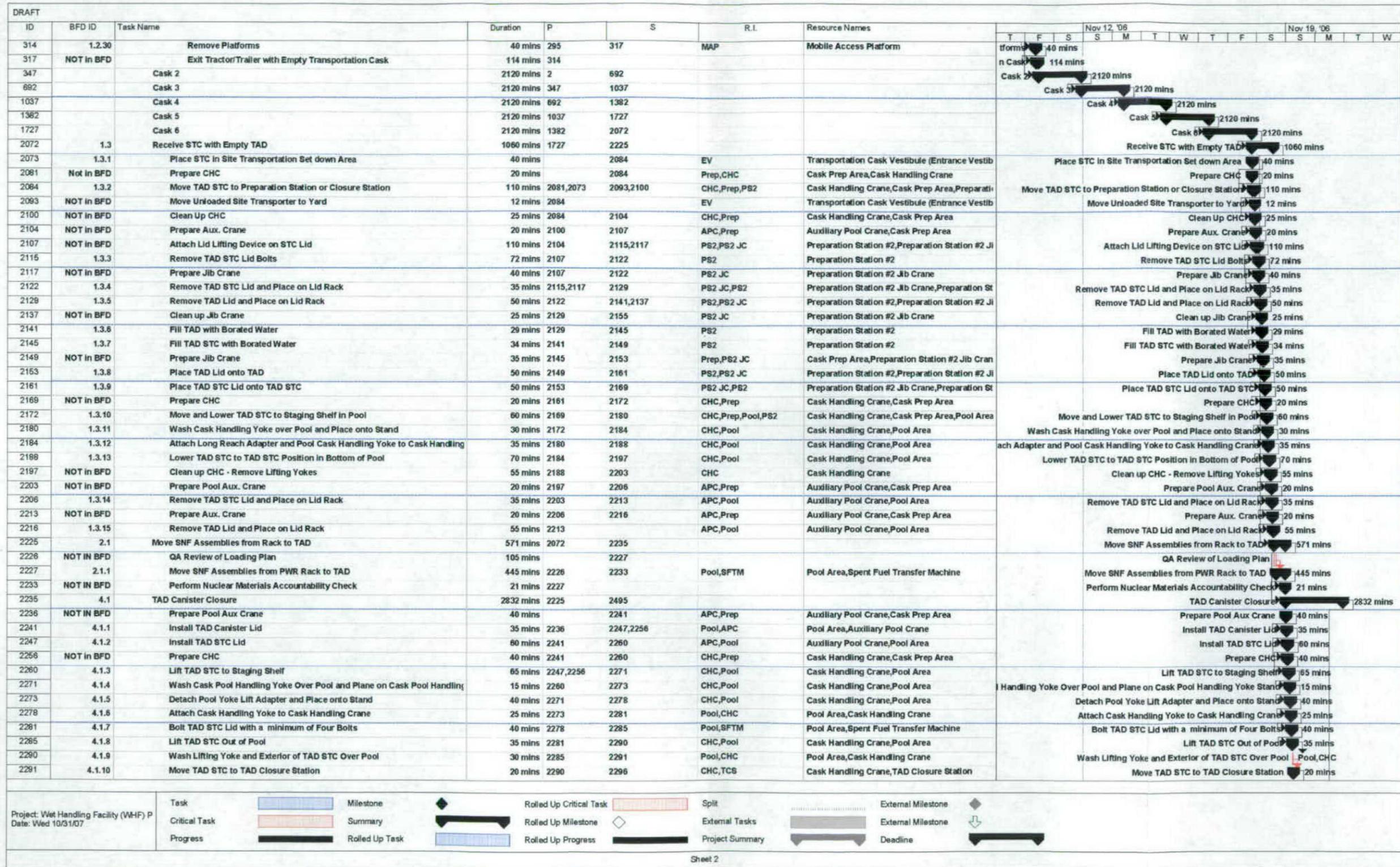


Figure A-2. Summary WHF Gantt Chart – Sheet 2

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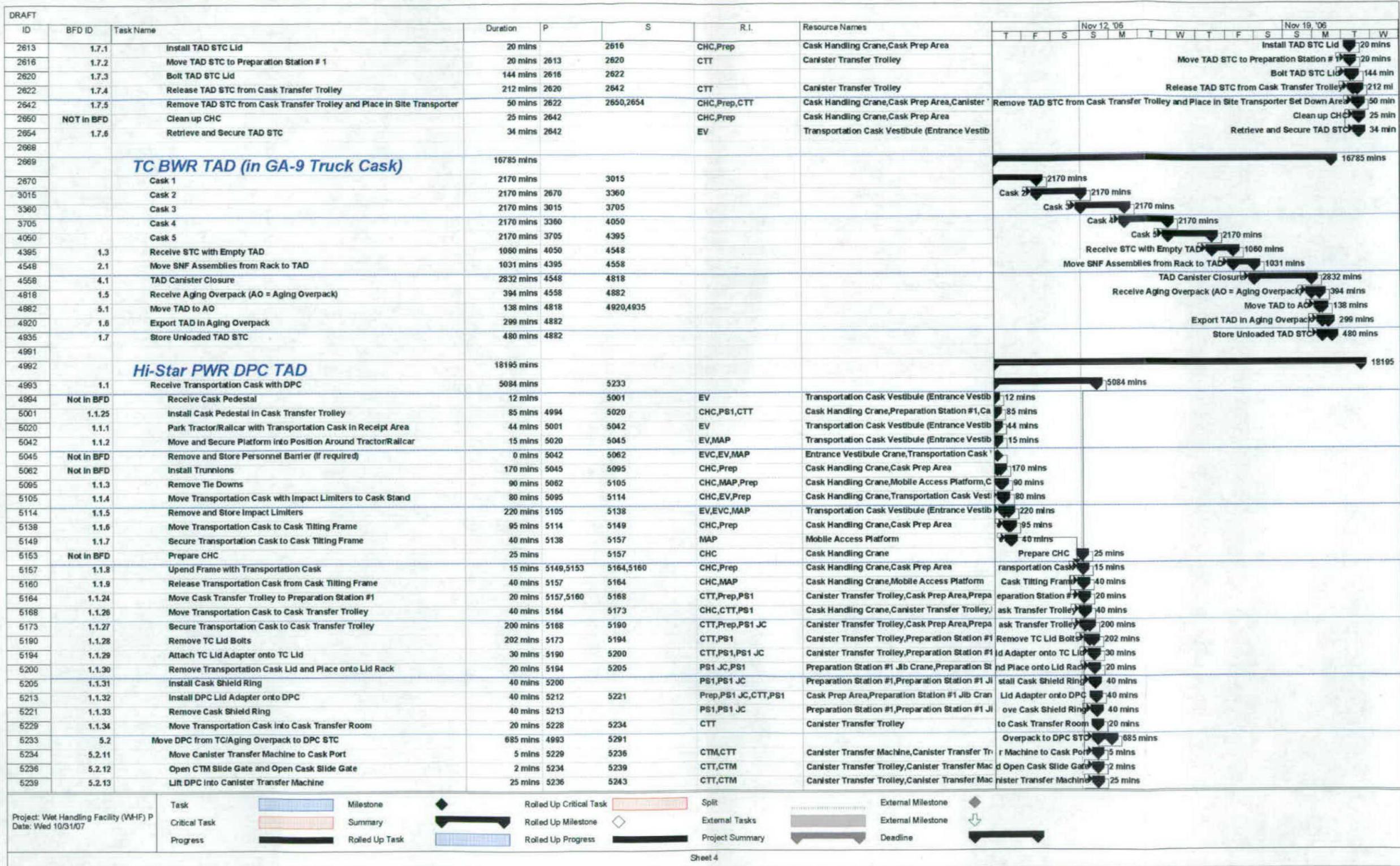


Figure A-4. Summary WHF Gantt Chart – Sheet 4

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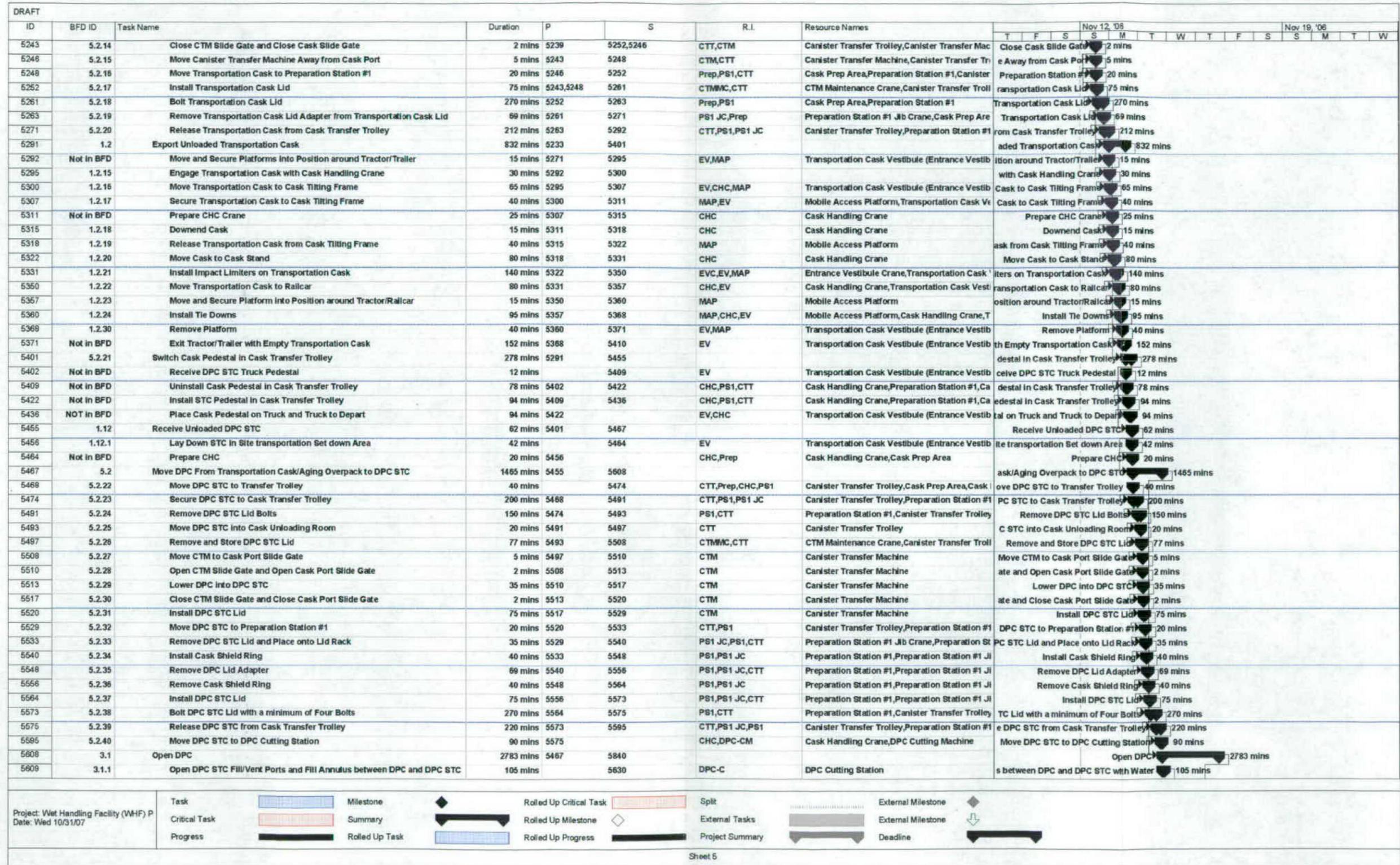


Figure A-5. Summary WHF Gantt Chart – Sheet 5

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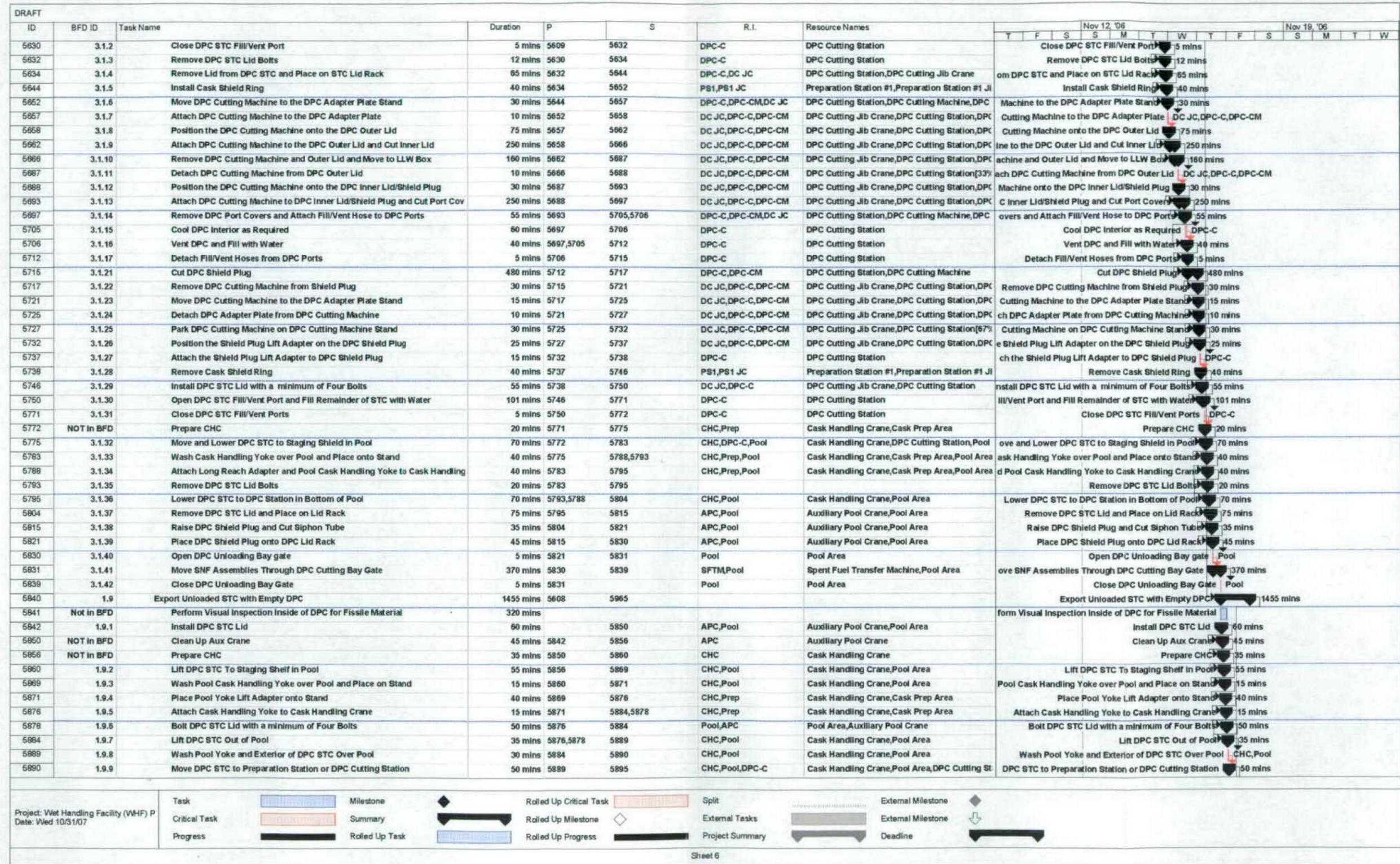


Figure A-6. Summary WHF Gantt Chart – Sheet 6

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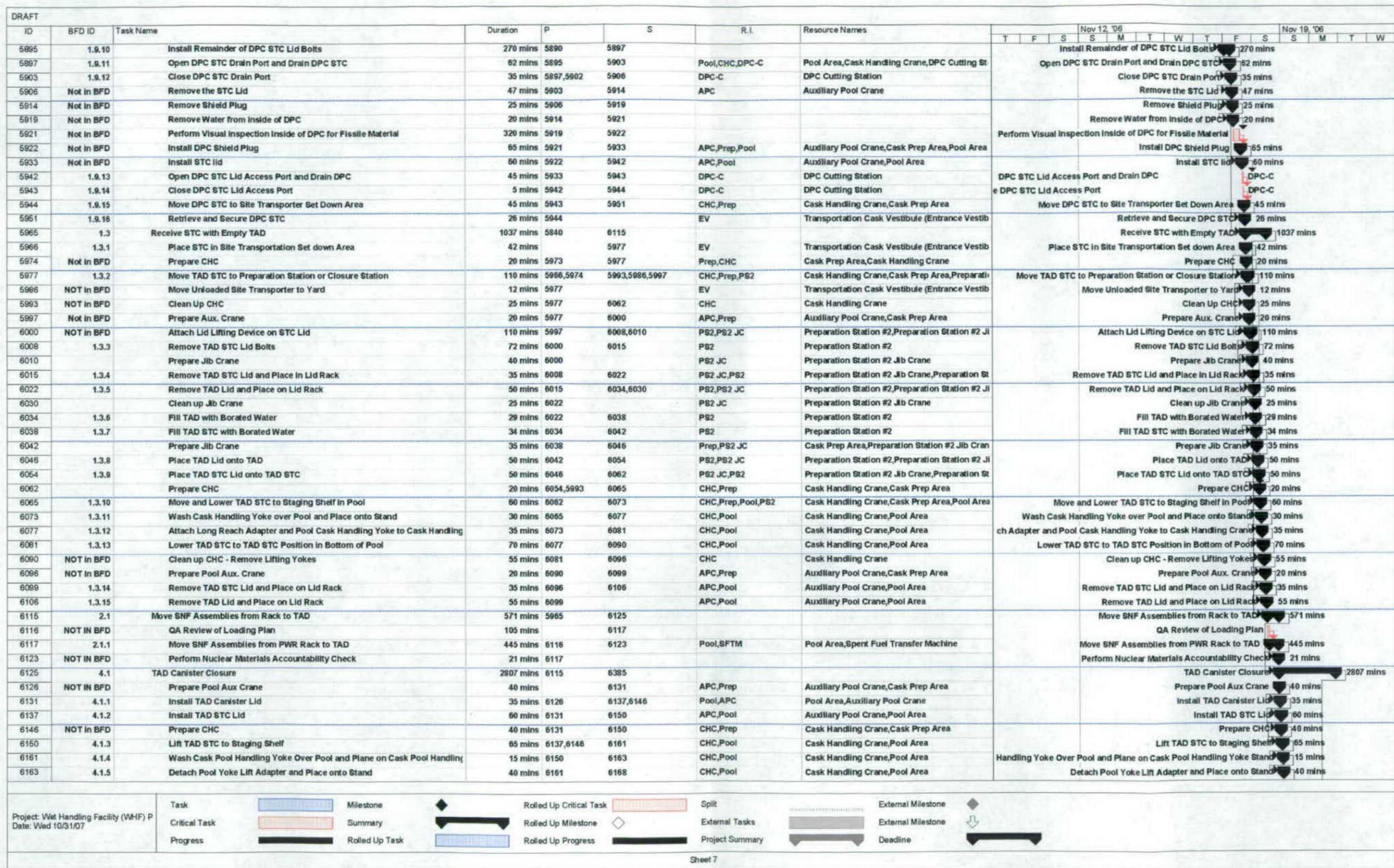


Figure A-7. Summary WHF Gantt Chart – Sheet 7

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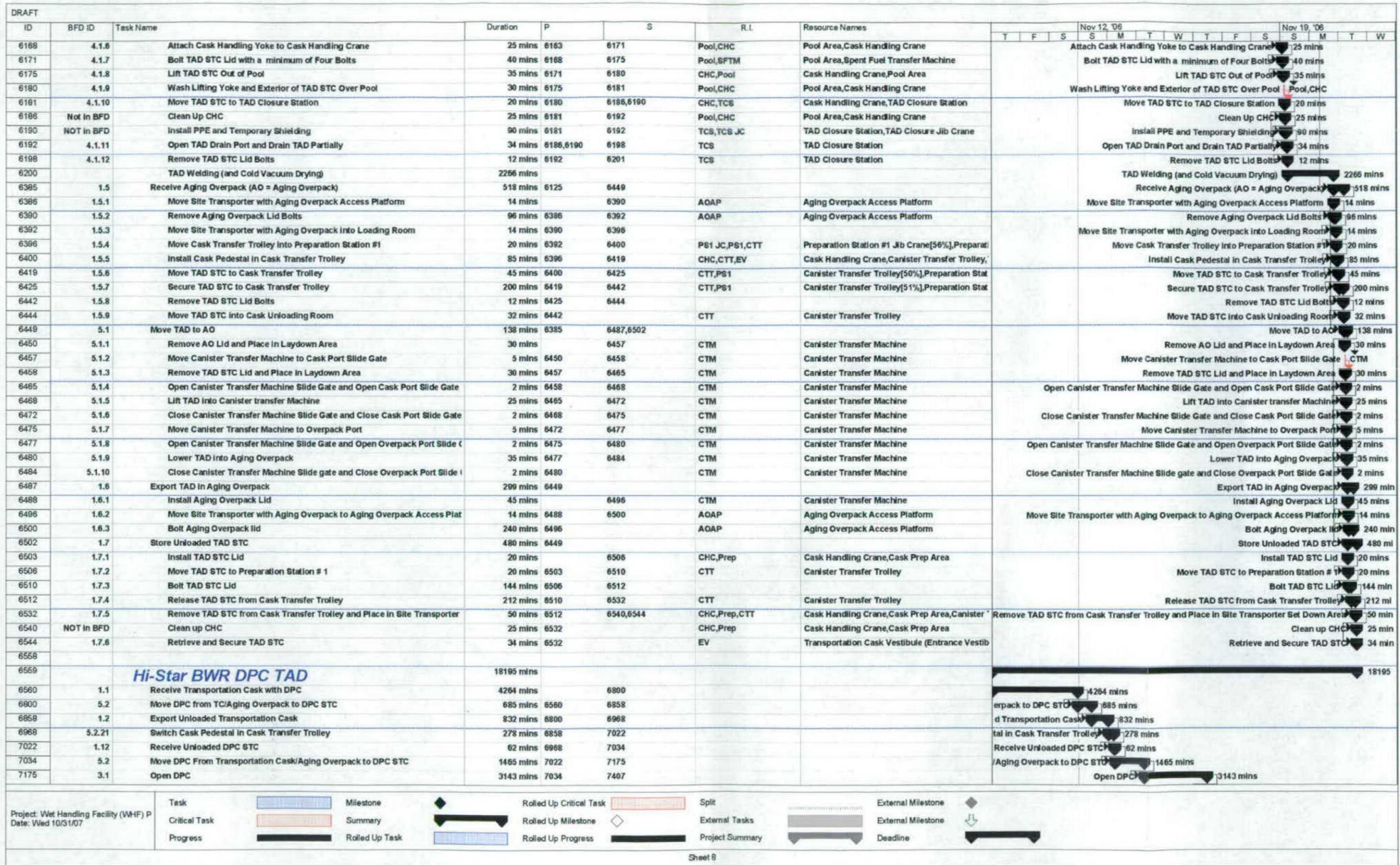


Figure A-8. Summary WHF Gantt Chart – Sheet 8

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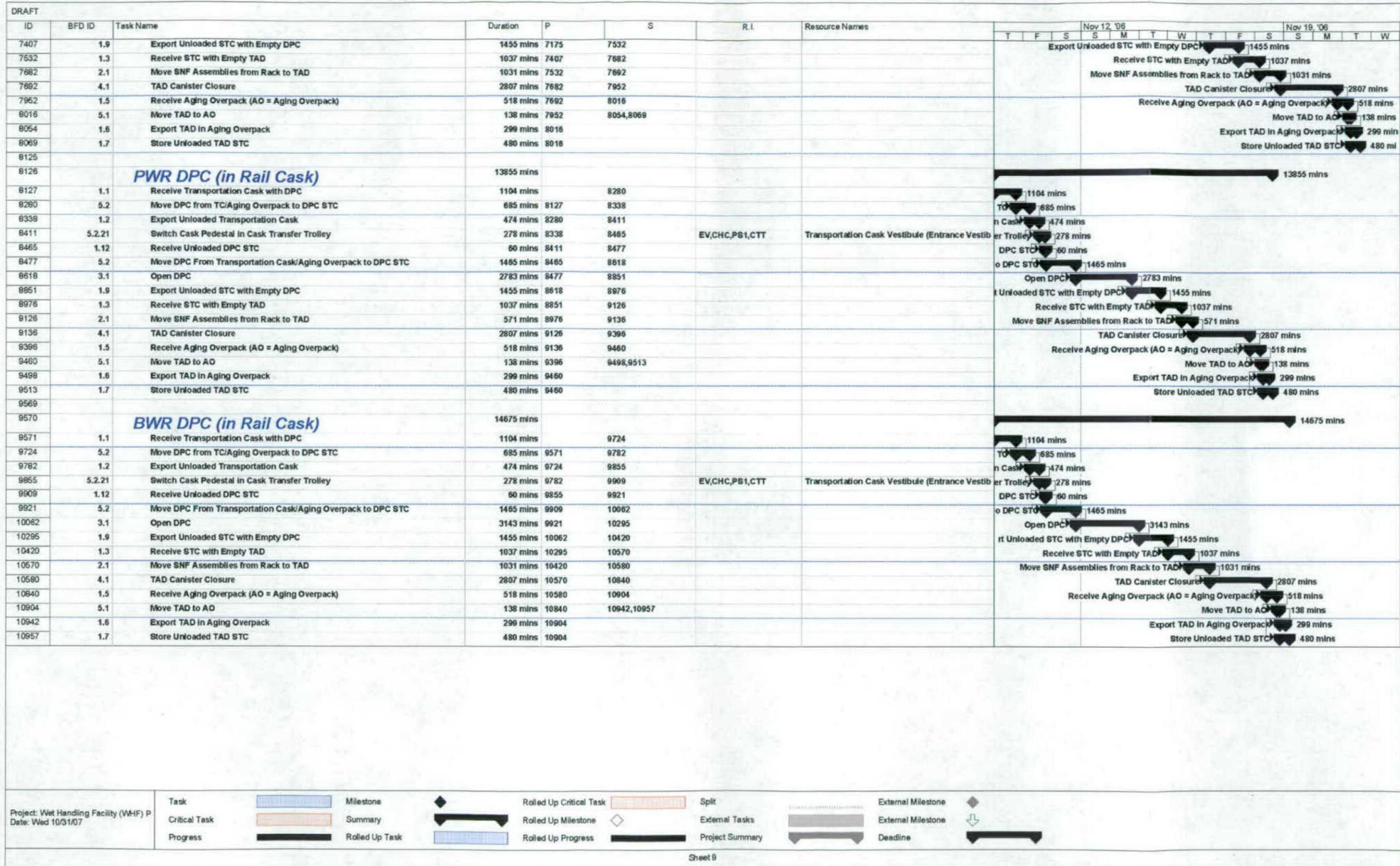


Figure A-9. Summary WHF Gantt Chart – Sheet 9

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**APPENDIX B -  
HOLTEC INTERNATIONAL EMAIL**

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Holtec Center, 555 Lincoln Drive West, Marlton, NJ 08053

Telephone (856) 797-0900

Fax (856) 797-0909

**SENT VIA E-MAIL ONLY**

March 15, 2007

Bechtel SAIC Company, LLC  
1180 N. Town Center Drive  
Las Vegas, NV 89144

Attention: Mr. Scott Estey

[scott\\_estey@vmp.gov](mailto:scott_estey@vmp.gov)

Phone: 702-821-7484

Reference: Yucca Mountain Project  
Design, Fabricate, and Furnish Helium Dehydrator for  
Transport, Aging, and Disposal Canister (TAD) Drying and Inerting System  
RFI No. ENG-07-013

Subject: Responses to Questions Posed During March 15, 2007 Telephone Call  
With John Griffiths

Dear Mr. Estey:

Holtec is pleased to once again assist you with the above referenced project.

Below are our responses to the questions posed during your telephone conversation today with John Griffiths, of Holtec.

**Question 1: Is an air cooled condensing module viable in an indoor application?**

*Holtec Response to Question 1: The air-cooled condensing module is the standard FHD design supplied to Holtec's nuclear clients. The heat rejected by the condensing module (180,000 to 200,000 BTU/hr) needs to be evaluated against the plant HVAC system to ensure that the system is not overloaded.*

**Question 2: What are the typical drying times seen for FHD?**

*Holtec Response to Question 2: Typical drying times are from 16 to 38 hours per canister, depending on the heat load of the canister and the operational practices of the site. TAD drying is expected to be of similar duration with high heat load canisters and well insulated canisters requiring a shorter duration drying time.*



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Mr. Scott Estey  
Bechtel SAIC Company, LLC  
March 15, 2007  
Page 2 of 2

**Question 3: How much water is typically removed in FHD drying?**

*Holtec Response to Question 3: Typical water recovered in drying Holtec systems is about 10 gallons. The bulk of the liquid water is removed during a carefully controlled canister blow-down process.*

Again, Holtec looks forward to working with Bechtel throughout the review process and to having the opportunity to bid on this project when the RFP is released.

Sincerely,

Kay Becnel  
Marketing Specialist

CC: Mr. A. Narayanan (Vijay) (Bechtel)  
Mr. John Griffiths (Holtec)  
Ms. Joy Russell (Holtec)

Document ID: 5633ab

**ATTACHMENT I-**  
**SIMCAD™ MODEL, GANTT CHARTS, RESULT FILES, AND FLOWCHARTS**

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## I.1 Listing of Electronic Files Contained on Compact Disk

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OFFICE OF CIVILIAN RADIOACTIVE WASTE MANAGEMENT  
SPECIAL INSTRUCTION SHEET

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This is a placeholder page for records that cannot be scanned.

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CD's 1 Original & 1 Copy

Validation of complete file transferred. All files copied. Software used: Excel

THIS IS AN ELECTRONIC  
ATTACHMENT

14. RPC Electronic Media Verification

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MD5 Validation

## I.1 Listing of Electronic Files Contained on Compact Disk

Directory of \Attachment I

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10/29/2007 12:02 PM <DIR> .
10/30/2007 04:13 PM <DIR> ..
10/25/2007 12:21 PM      19,202,560 WHF-rev02-102507-STCin-12h00m.SIM
10/25/2007 05:24 PM      102,912 Case_1_(Avg)_output.xls
10/25/2007 05:47 PM      105,984 Case_4_output.xls
10/25/2007 05:57 PM      107,520 Case_5_output.xls
10/25/2007 05:36 PM      109,056 Case_3_output.xls
10/25/2007 06:16 PM      109,568 Case_7_output.xls
10/25/2007 06:36 PM      114,176 Case_9_output.xls
10/25/2007 06:06 PM      114,688 Case_6_output.xls
10/25/2007 06:26 PM      119,296 Case_8_output.xls
10/25/2007 04:31 PM      124,928 Case_2_(Peak)_output.xls
10/25/2007 06:47 PM      152,576 Case_10_output.xls
10/25/2007 06:59 PM      187,904 Case_11_output.xls
10/25/2007 07:12 PM      195,072 Case_12_output.xls
09/13/2007 04:17 PM      113,908 050mh0h00000208.pdf
09/13/2007 04:24 PM      123,197 050mh0h00000211.pdf
09/13/2007 04:17 PM      124,112 050mh0h00000207.pdf
09/13/2007 04:30 PM      126,297 050mh0h00000214.pdf
09/13/2007 04:30 PM      127,046 050mh0h00000213.pdf
09/13/2007 04:03 PM      127,295 050mh0h00000202.pdf
09/13/2007 04:30 PM      127,807 050mh0h00000217.pdf
09/13/2007 04:18 PM      129,039 050mh0h00000209.pdf
09/13/2007 04:24 PM      130,763 050mh0h00000212.pdf
09/13/2007 04:17 PM      134,916 050mh0h00000206.pdf
09/13/2007 04:16 PM      140,225 050mh0h00000205.pdf
09/13/2007 04:30 PM      143,725 050mh0h00000215.pdf
09/13/2007 04:30 PM      145,922 050mh0h00000216.pdf
09/13/2007 04:07 PM      149,441 050mh0h00000204.pdf
09/13/2007 04:18 PM      158,245 050mh0h00000210.pdf
09/13/2007 04:05 PM      159,359 050mh0h00000203.pdf
09/13/2007 04:00 PM      394,488 050mh0h00000201.pdf
10/31/2007 12:22 PM      143,342,080 WHF Throughput Layout Rev02-
                    102407_15h_05m_FINAL.mpp
10/31/2007 12:25 PM           146 dir.txt
02/26/2007 04:10 PM      29,298,176 Waste Stream Evaluation.xls
10/29/2007 09:24 AM      29,184 Summary Output.xls

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34 File(s) 195,971,611 bytes